Microwave Circuits and Antenna Design



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Notation

c = speed of light in free space

 $\lambda_0 =$ wavelength of free space

 $k_0 =$ wavenumber of free space

 $k_1 =$ wavenumber of substrate

 $\eta_0 =$ intrinsic impedance of free space

 η_1 = intrinsic impedance of substrate

 \mathcal{E}_r = relative permittivity (dielectric constant) of substrate

 $\mathcal{E}_r^{e\!f\!f} = \text{effective relative permittivity}$ (accouting for fringing of flux lines at edges)

 \mathcal{E}_{rc}^{eff} = complex effective relative permittivity (used in the cavity model to account for all losses) $c = 2.99792458 \times 10^{8} \text{ [m/s]}$ $\lambda_{0} = c / f$ $k_{0} = \omega \sqrt{\mu_{0}\varepsilon_{0}} = 2\pi / \lambda_{0}$ $k_{1} = k_{0} \sqrt{\varepsilon_{r}}$ $\eta_{0} = \sqrt{\frac{\mu_{0}}{\varepsilon_{0}}} \approx 376.7303 \text{ [}\Omega\text{]}$ $\eta_{1} = \eta_{0} / \sqrt{\varepsilon_{r}}$

$$c = \frac{1}{\sqrt{\varepsilon_0 \mu_0}}$$

$$\mu_0 = 4\pi \times 10^7 \text{ [H/m]}$$

$$\varepsilon_0 = \frac{1}{\mu_0 c^2} \approx 8.854188 \times 10^{12} \text{ [F/m]}$$

Antenna

- Anten, hava ile elektronik cihazlar arasındaki geçiş yapısıdır. Antenler, elektrik sinyallerini havaya elektromanyetik dalga olarak ışırlar, havadaki elektromanyetik sinyalleri ise elektrik sinyaline dönüştürürler.
- A usually metallic device (as a rod or wire) is used for radiating or receiving electromagnetic waves. An antenna is a transitional structure between free-space and a guiding structure (Balanis; Antenna Theory). Ortamda ortama geçişin efekif alanı, antenin efektif ışıma alanıdır.
- Antenna is a device that converts electrons into photons or vice versa. A transmitting antenna converts electrons into photons while a receiving antenna converts photons into electrons.
- The beam width of an antenna measure at half of the maximum power received by an antenna or the 3 dB beam width of the antenna is termed as half null beam width.
- Power radiated from an antenna per unit solid angle is called radiation intensity. Unit of radiation intensity is watts per steridian or per square degree.

Antenna Performance Parameters

Antenna parameters

- Radiation resistance
- Directivity
- Antenna gain
- Beamwidth
- Effective aperture
- Friis transmission equation

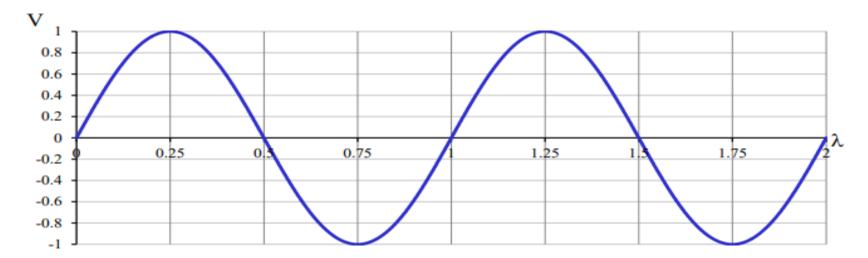
 $=\frac{G_t G_r \lambda^2}{\left(4\pi R\right)^2}$ $\frac{P_r}{P_t}$ $-\overline{\lambda^2 R^2}$

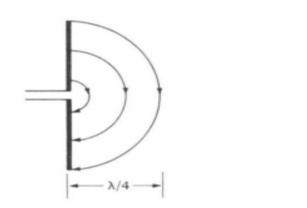
Antenna Performance Parameters

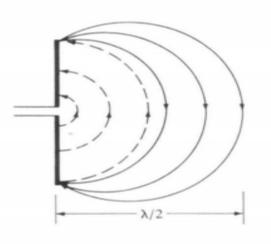
- Common antenna performance parameters include:
 - Return Loss Impedance
 - Gain and Directivity
 - Frequency coverage
 - Bandwidth
 - Beamwidth
 - Polarization
 - Efficiency
 - Field Patterns
 - Front to Back Ratio and Side loobes

Antenna Basics

- How is radiation achieved?
- Wavelength is key: $\frac{\lambda}{2}$, where $\lambda = \frac{c_o}{f_r \sqrt{\epsilon_r}}$



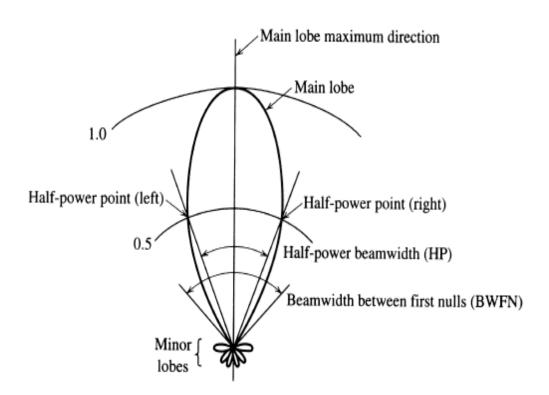






Beamwidth ($\theta_{\rm B}, \Phi_{\rm B}$)

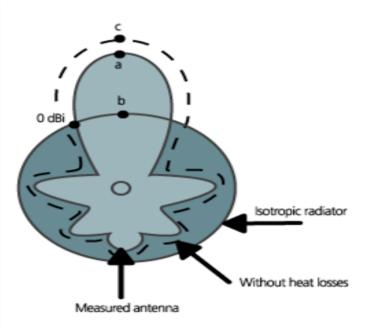
- Beamwidth (θ_B , Φ_B) of an antenna is the angle defined by the points either side of boresight at which the power is reduced by 3-dB, for a given plane.
 - For example if θ_B , represents the beamwidth in the horizontal plane, Φ_B represents the beamwidth in the orthogonal (vertical) plane.
 - The 3-dB (Gücün yarıya düştüğü) beamwidth defines the half-power beam.



dBi versus dBd

•dBi indicates gain vs. isotropic antenna •Isotropic antenna radiates equally well in all directions, spherical pattern, Gain=1, Gain(dBi))=0 dBi

•dBd indicates gain vs. reference half-wavelength dipole•Dipole has a doughnut shaped pattern with a gain of 2.15 dBi



dBi = dBd + 2.15 dB

Antenna Gain

• Relationship between antenna gain and effective area

$$G = \frac{4\pi A_e}{\lambda^2} = \frac{4\pi f^2 A_e}{c^2}$$

- G =antenna gain
- A_e = effective area
- f = carrier frequency
- $c = speed of light (3 \times 10^8 m/s)$
- $\lambda = \text{carrier wavelength}$

ANTENNA BASICS

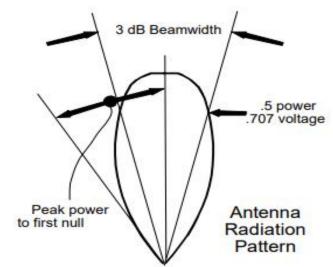
1. The Gain of an antenna with losses is given by:

$$G \approx \frac{4\pi\eta A}{\lambda^2} \quad Where \quad \begin{array}{l} \eta = Efficiency \\ A = Physical \ aperture \ area \\ \lambda = wavelength \end{array} \quad \begin{array}{l} another \ is: \\ G = \frac{1}{B} \end{array}$$

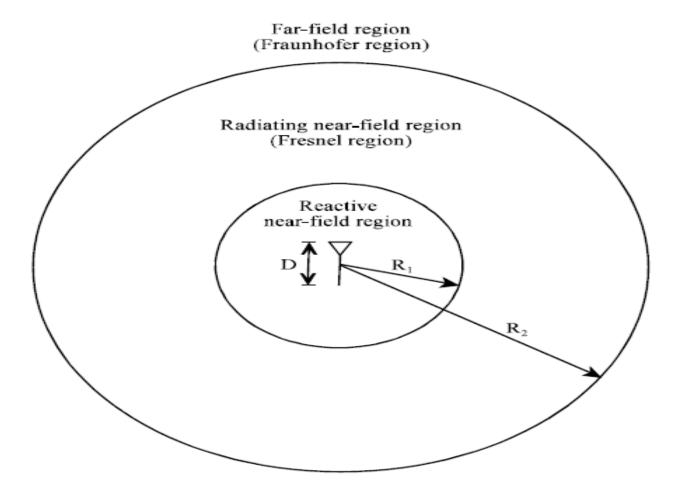
Where
$$BW_{\theta and \phi}$$
 are the elev & az
beamwidths in degrees.
For approximating an antenna pattern with:
(1) A rectangle; X=41253, $\eta_{typical} = 0.7$
(2) An ellipsoid; X=52525, $\eta_{typical} = 0.55$

 $G = \frac{X \eta}{BW_{\phi} BW_{\theta}}$

- Gain of rectangular X-Band Aperture
 G = 1.4 LW Where: Length (L) and Width (W) are in cm
- 3. Gain of Circular X-Band Aperture $G = d^2\eta$ Where: $d = antenna \ diameter \ in \ cm$ $\eta = aperture \ efficiency$
- 4. Gain of an isotropic antenna radiating in a uniform spherical pattern is one (0 dB).
- 5. Antenna with a 20 degree beamwidth has a 20 dB gain.
- 6. 3 dB beamwidth is approximately equal to the angle from the peak of the power to the first null (see figure at right).
- 7. Parabolic Antenna Beamwidth: $BW = \frac{70\lambda}{d}$ Where: BW = antenna beamwidth; λ = wavelength; d = antenna diameter.



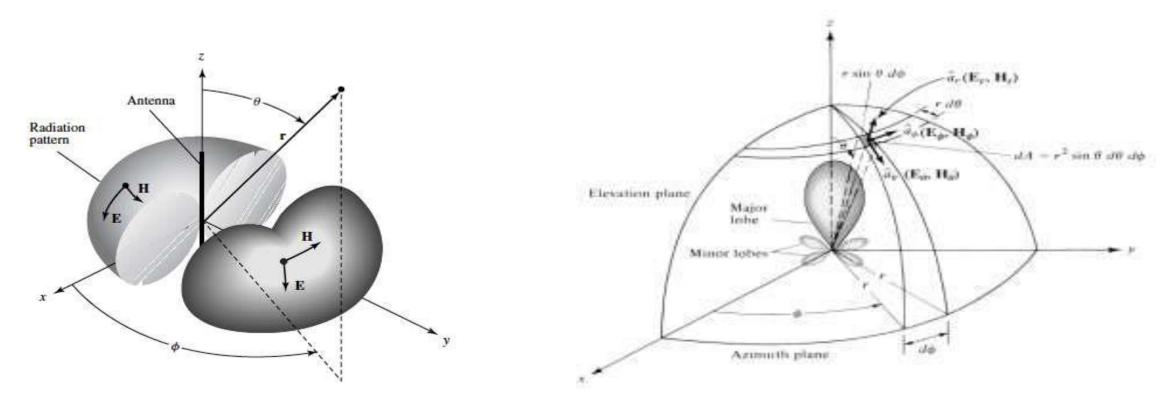
Antenna Field Regions



D = maximum antenna dimension

$$R_1 = 0.62 \sqrt{\frac{D^3}{\lambda}}$$
$$R_2 = \frac{2D^2}{\lambda}$$

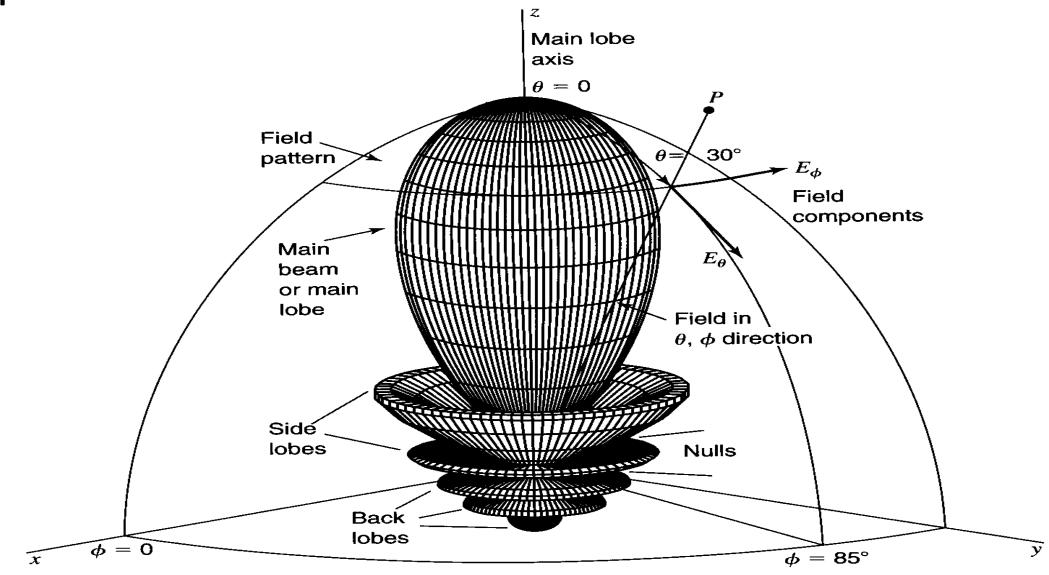
Pattern of antennas



Isotropic, directional, and omnidirectional pattern

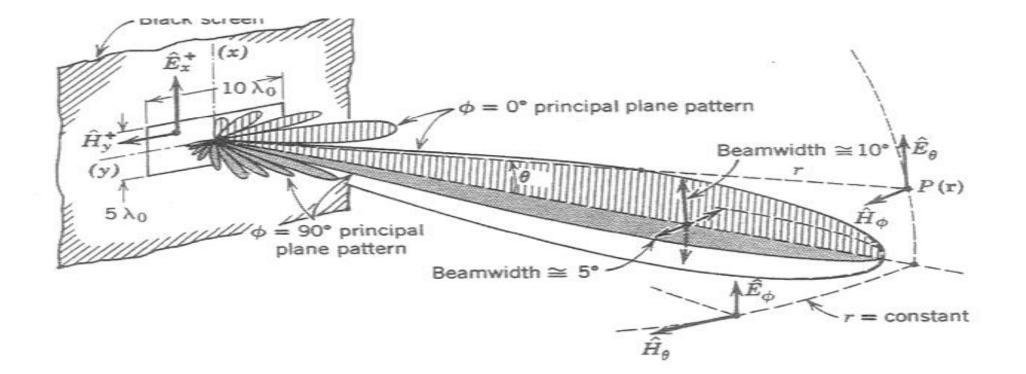
Radiation pattern

Radiation pattern

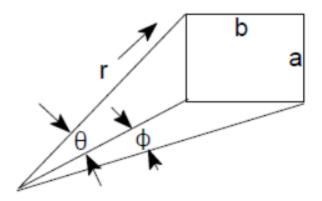


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Antenna Pattern 3D



Approximating the antenna pattern as a rectangular area:



$$a = r \sin \theta, \quad b = r \sin \phi, \text{ area} = ab = r^{2} \sin \theta \sin \phi$$

$$G = \frac{Area \text{ of Sphere}}{Area \text{ of Antenna pattern}} = \frac{4\pi r^{2}}{r^{2} \sin \theta \sin \phi} = \frac{4\pi}{\sin \theta \sin \phi}$$
For small angles, $\sin \phi = \phi$ in radians, so:

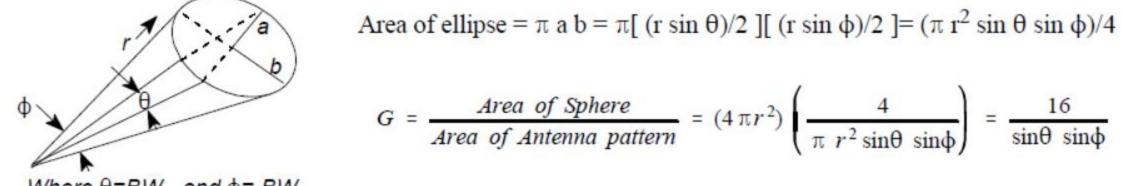
Where $\theta = BW_{\theta}$, and $\varphi = BW_{\phi}$

$$G = \frac{4 \pi}{\sin \phi \sin \theta} = \frac{4 \pi}{\phi \theta (radians)} = \frac{4 \pi}{\phi \theta} \left(\frac{360^{\circ} \ 360^{\circ}}{2 \pi \ 2 \pi} \right) = \frac{41253}{\phi \theta (degrees)} \text{ or } \frac{41253}{BW_{\phi} \ BW_{\theta} (degrees)}$$

The second term in the equation above is identical to equation [3].

Converting to dB,
$$G_{\max}(dB) = 10 \log \left[\frac{41253}{BW_{\phi} BW_{\theta}}\right]$$
 with BW_{ϕ} and BW_{θ} in degrees

Approximating the antenna pattern as an elliptical area:



$$G = \frac{Area \ of \ Sphere}{Area \ of \ Antenna \ pattern} = (4 \ \pi r^2) \left(\frac{4}{\pi \ r^2 \sin\theta \ \sin\phi}\right) = \frac{16}{\sin\theta \ \sin\phi}$$

Where $\theta = BW_{\theta}$, and $\varphi = BW_{\phi}$

For small angles,
$$\sin \phi = \phi$$
 in radians, so:

$$G = \frac{16}{\sin \phi \sin \theta} = \frac{16}{\phi \theta (radians)} = \frac{16}{\phi \theta} \left(\frac{360^{\circ} \ 360^{\circ}}{2 \pi \ 2 \pi} \right) = \frac{52525}{\phi \theta (degrees)} \text{ or } \frac{52525}{BW_{\phi} \ BW_{\theta} (degrees)}$$

For a very directional radar dish with a beamwidth of 1° and an average efficiency of 55%:

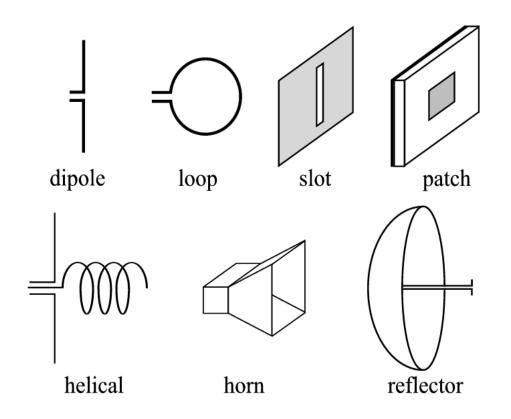
Ideally: G = 52525, or in dB form: 10 log G =10 log 52525 = 47.2 dB

With efficiency taken into account, G = 0.55(52525) = 28888, or in log form: $10 \log G = 44.6 \text{ dB}$

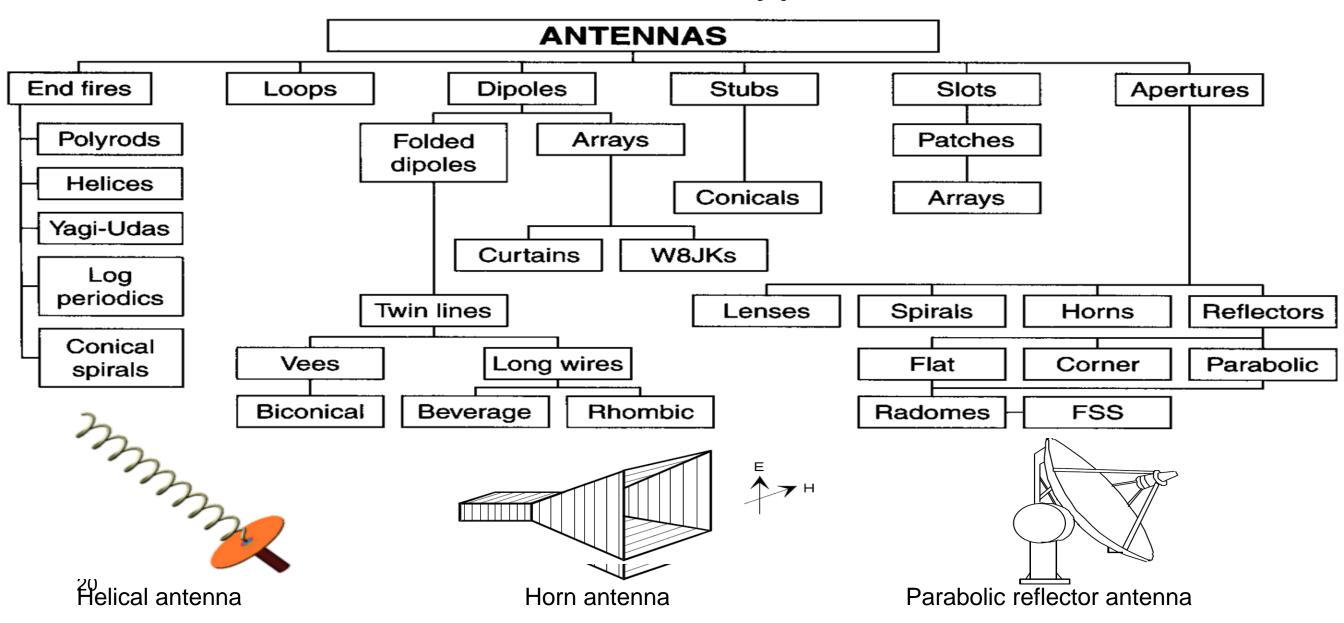


Types of Antennas

- Wire antennas
- Aperture antennas
- Array antennas
- Reflector antennas
- Lens antennas
- Patch antennas



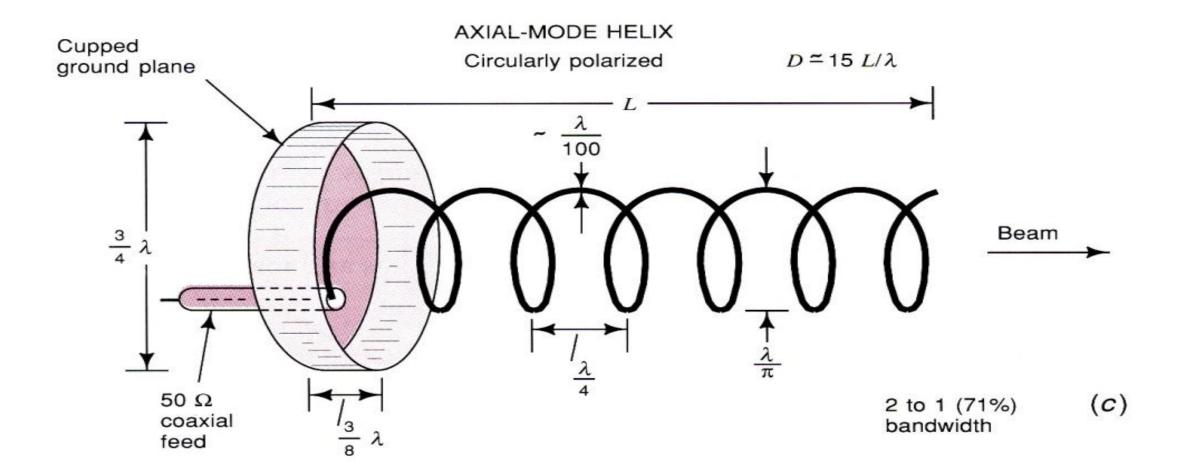
Antennas come in a wide variety of sizes and shapes Antenna types



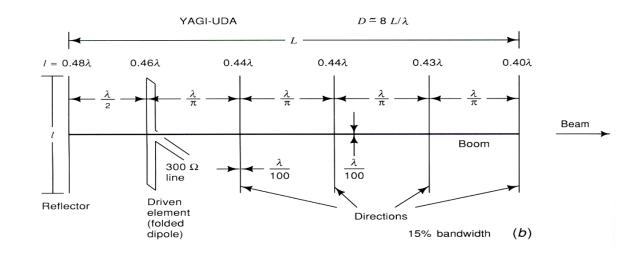
Different Antennas







Yagi-Uda

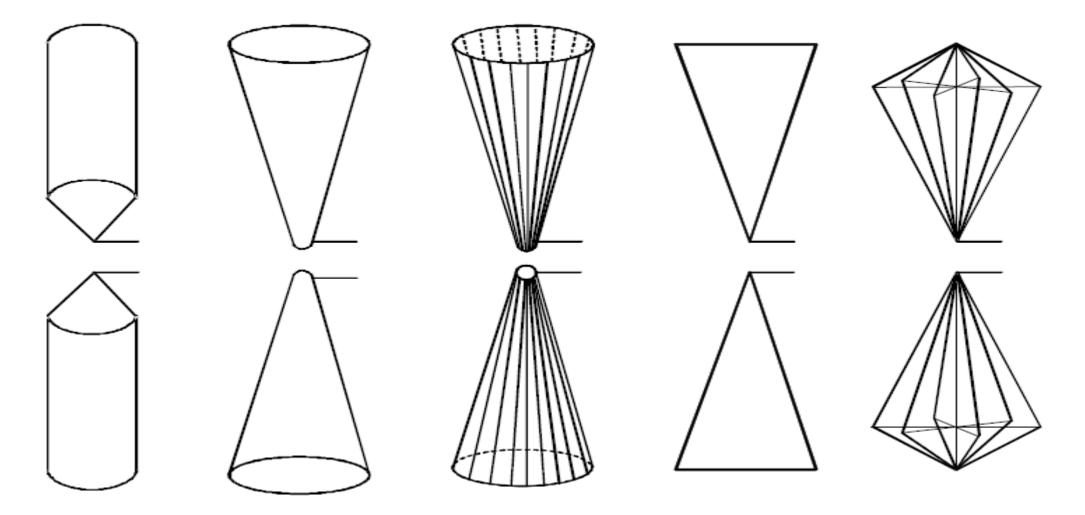




3-Element Yagi AO 6.5	330°	30°	ground Azimuth	3-Element Yagi AO 6.5		ground
300° 270°	-10 -20 -30 -40		60° 90°	12 150° 180°	90° 60° -40-30 -20 -10 dB	0°
14.0° Elevation 0 dB = 13.35 dBi	210*	150*	14.175 MHz	90.0° Azimuth 0 dB = 13.35 dBi	Elevation 14	.175 MHz

Elements	Gain dBi	Gain dBd
3	7.5	5.5
4	8.5	6.5
5	10	8
6	11.5	9.5
7	12.5	10.5
8	13.5	11.5

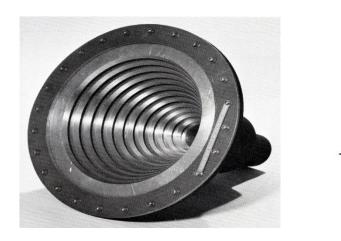
Dipole antennas

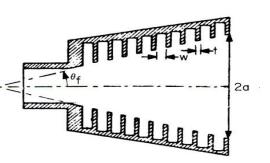


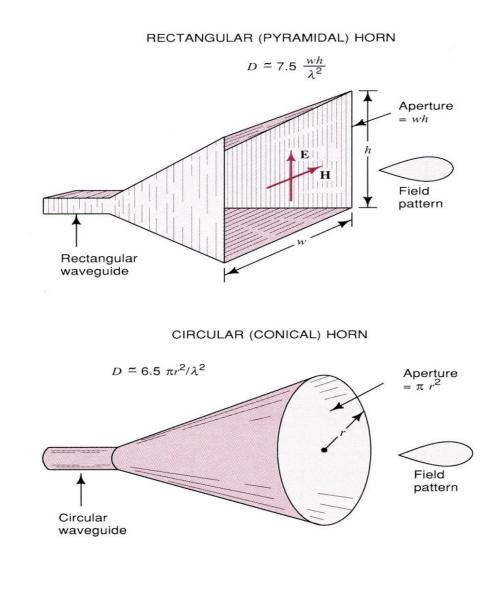
Versions of broadband dipole antennas

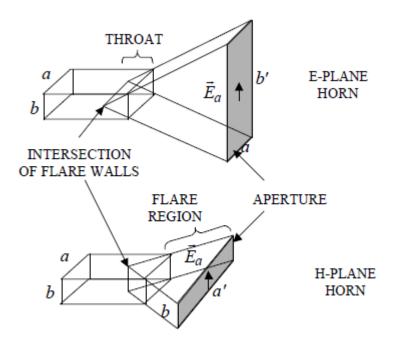
Horn antenna

- Rectangular or circular waveguide flared up
- Spherical wave fronts from phase centre
- Flare angle and aperture determine gain
- •Aperture antennas derived from waveguide technology (circular, rectangular)
- •Can transfer high power (magnetrons, klystrons)
- •Above few GHz
- •Will be explored inprace during the school









The aperture dimensions of a pyramidal horn are 12x6 cm and operating at a frequency of 10 GHz. Find the beam width and directivity.

Frequency = 10 GHz $\lambda = \frac{3 \times 10^8}{10 \times 10^9} = 3 \, cm$ d = 12 cm and w = 6 cmBeamwidth: $\phi_E = 56 \frac{\lambda}{d} = 14^{\circ}$ $\phi_H = 67 \frac{\lambda}{w} = 33.5^{\circ}$ $powergain = \frac{4.5wd}{a^2} = 36 = 15.56dB$

$$Directivity = \frac{7.5wd}{\lambda^2} = 60$$

Horn Example

Example: An E-plane horn has $R_1 = 20\lambda$ and $a = 0.5\lambda$.

(a) The optimum aperture dimension for maximum directivity

$$b' = \sqrt{2\lambda R_{1E}} = \lambda\sqrt{40} = 6.3\lambda$$

(b) The flare angle for the optimum directivity

$$\tan(\psi/2) = \frac{b'/2}{R_1} = \frac{6.3\lambda/2}{20\lambda} = 0.1575$$
$$\psi/2 = 8.95^{\circ}$$
$$\psi = 17.9^{\circ}$$

(c) The optimum directivity is

$$D_{\text{opt}} = 10.2 \frac{(0.5\lambda)(6.3\lambda)}{\lambda^2} \left(\frac{1}{1.25}\right) = 25.7 = 14.1 \text{ dB}$$

Parabolic conducting reflector Geometry and operation

For a parabolic conducting reflector surface of focal length *f* with a feed at the focus *F*.

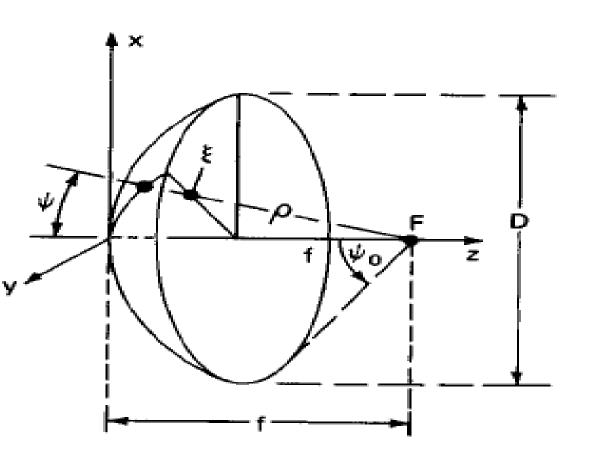
In rect. coordinates

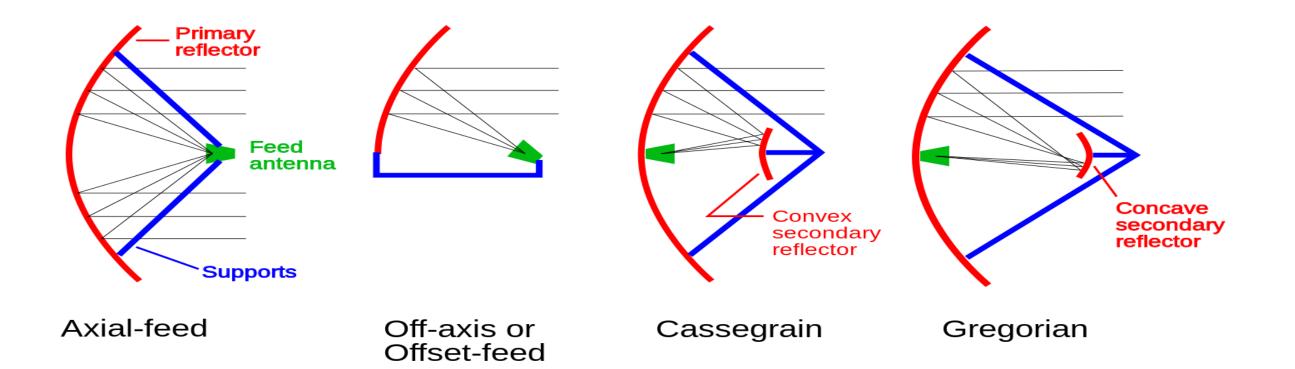
 $z = (x^2 + y^2)/4f$

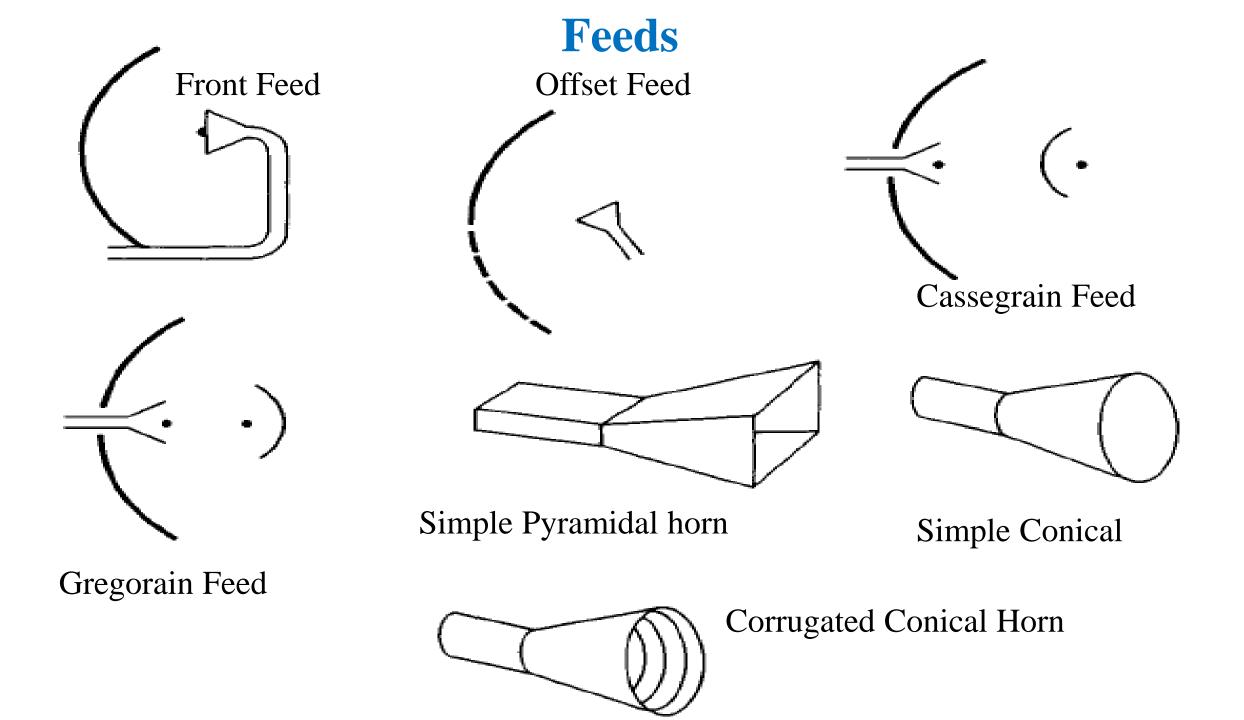
In spherical coordinates

 $\rho = f \sec^2 \psi/2$

 $\tan\psi_o/2 = D/4f$



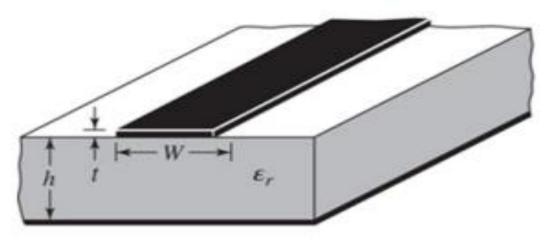




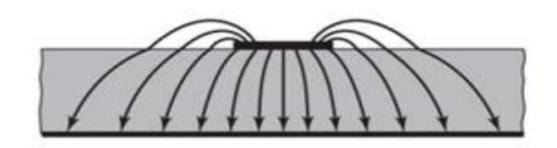
Microstrip Antenna Design

Micro-strip Antenna

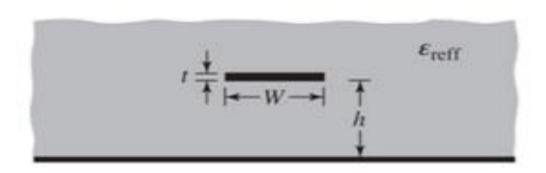
- What is Micro-strip Antenna ?
- A Micro-strip patch antenna consists of a radiating patch on one side of a dielectric substrate which has a ground plane on the other side.
- Invented by Bob Munson in 1972 (but earlier work by Dechamps goes back to1953).



(a) Microstrip line

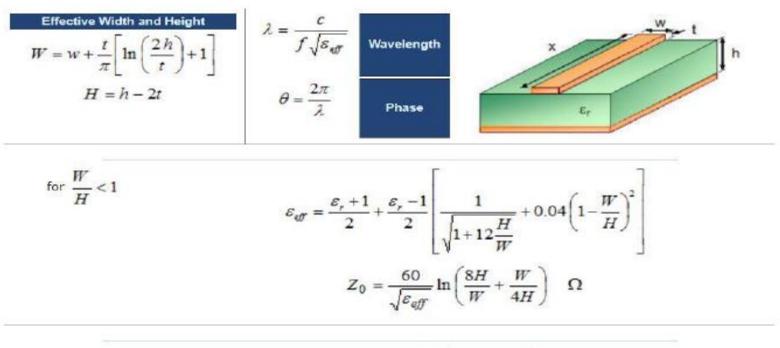


(b) Electric field lines



(c) Effective dielectric constant

Rectangular Microstrip Feedline formul



for
$$\frac{W}{H} \ge 1$$

$$\mathcal{E}_{eff} = \frac{\mathcal{E}_{r} + 1}{2} + \frac{\mathcal{E}_{r} - 1}{2\sqrt{1 + 12\frac{H}{W}}}$$

$$Z_{0} = \frac{120 \pi}{\sqrt{\mathcal{E}_{eff}} \left[\frac{W}{H} + 1.393 + \frac{2}{3} \ln\left(\frac{W}{H} + 1.444\right)\right]} \quad \Omega$$

The characteristic impedance of the microstrip may be written as

$$Z_o = \begin{cases} \frac{60}{\sqrt{\varepsilon_e}} \ln\left(\frac{8d}{W} + \frac{W}{4d}\right) & W/d \le 1\\ \frac{120\pi}{\sqrt{\varepsilon_e} [W/d + 1.393 + 0.667\ln(W/d + 1.444)]} & W/d \ge 1 \end{cases}$$

Solving this equation for W/d yields

$$\frac{W}{d} = \begin{cases} \frac{8e^{A}}{e^{2A} - 2} & W/d \le 2\\ \frac{2}{\pi} \left[B - 1 - \ln(2B - 1) + \frac{\varepsilon_r - 1}{2\varepsilon_r} \left\{ \ln(B - 1) + 0.39 - \frac{0.61}{\varepsilon_r} \right\} \right] & W/d \ge 2 \end{cases}$$

where

$$\begin{split} A &= \frac{Z_o}{60} \sqrt{\frac{\varepsilon_r + 1}{2}} + \frac{\varepsilon_r - 1}{\varepsilon_r + 1} \left(0.23 + \frac{0.11}{\varepsilon_r} \right) \\ B &= \frac{377 \pi}{2 Z_o \sqrt{\varepsilon_r}} \end{split}$$

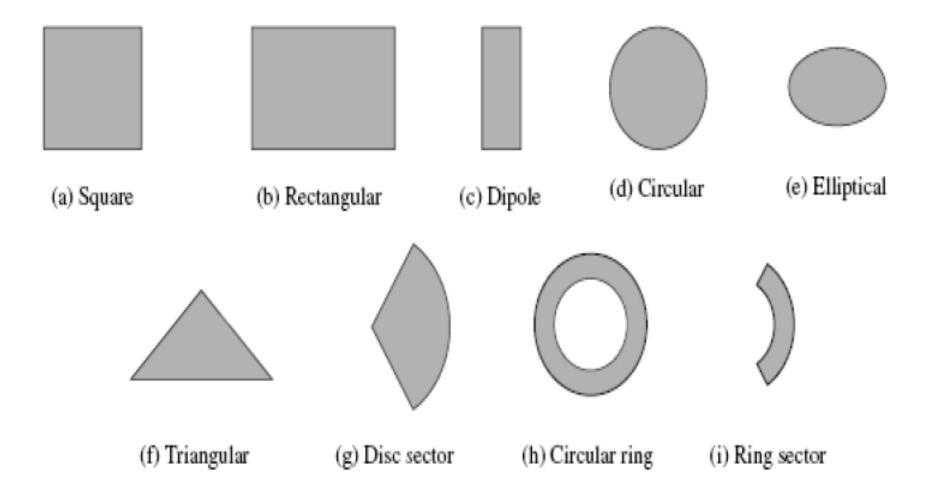
Microstrip Antenna Applications

- Used in mobile satellite communication system.
- Direct broad cast telivision(DBS).
- Wire less LAN'S.
- Feed elements in coaxial system
- GPS system.
- Missiles and telementry
- UHF Patch Antennas for Space

Why we use Microstrip Patch Antennas ?

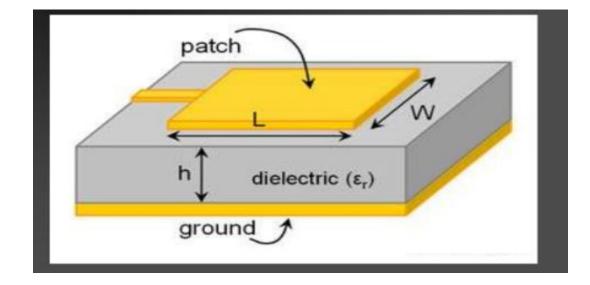
- Flat surface makes them ideal for mounting on airplane
- Impedance matching fairly simple
- Microstrip patch antennas have a very high antenna quality factor(Q).
- Q represents the losses associated with the antenna and a large Q leads to narrow bandwidth and low efficiency.
- Q can be reduced by increasing the thickness of the dielectric substrate. But as the thickness increases, an increasing fraction of the total power delivered by the source goes into a surface wave
- UHF Patch antenna
- UHF Patch Antennas for Space
- These antennas are capable of supporting high data rates to at least 10 Watts of transmitted power.

Shapes of Microstrip Patch



Feeding Techniques

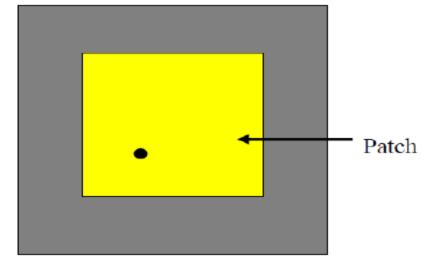
- Coaxial feed
- Microstrip feed
- Proximity coupled microstrip feed
- Aperture coupled microstrip feed
- Coplanar wave guide
- Line Feed



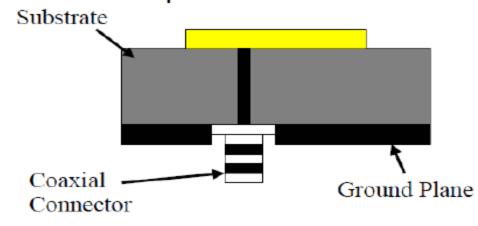
1-Microstrip Line Feed : In this type of feed technique, a conducting strip is connected directly to the edge of the microstrip patch. This kind of feed arrangement has the advantage that the feed can be etched on the same substrate to provide a planar structure.

2-Coaxial Feed

- The Coaxial feed or probe feed is a very common technique used for feeding Microstrip patch antennas.
- The main advantage of this type of feeding scheme is that the feed can be placed at any desired location inside the patch in order to match with its input impedance.
- This feed method is easy to fabricate and has low spurious radiation.
- However, its major disadvantage is that it Coaxia Ground Plane Connector Substrate Patch provides narrow bandwidth and is difficult to model since a hole has to be drilled in the substrate . and the connector protrudes outside the ground plane, thus not making it completely planar for thick substrates .



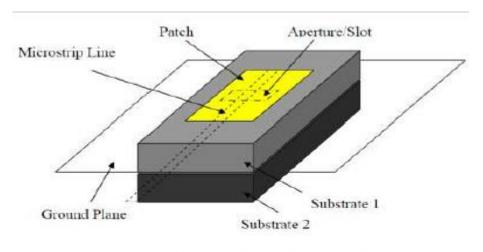
Probe fed Rectangular Microstrip Patch Antenna from top



Probe fed Rectangular Microstrip Patch Antenna from side view

3-Aperture Coupled Feed

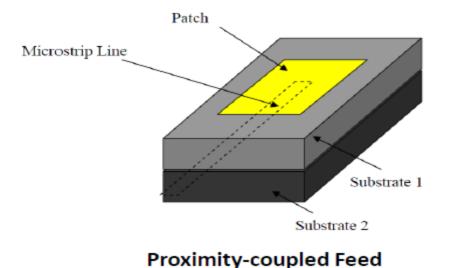
- In this type of feed technique, the radiating patch and the microstrip feed line are separated by the ground plane .
- Coupling between the patch and the feed line is made through a slot or an aperture in the ground plane.
- The coupling aperture is usually centered under the patch, leading to lower cross polarization due to symmetry of the configuration.
- The amount of coupling from the feed line to the patch is determined by the shape, size and location of the aperture.



Aperture-coupled feed

4-Proximity Coupled Feed

- This type of feed technique is also called as "the electromagnetic coupling scheme".
- The main advantage of this feed technique is that it eliminates spurious feed radiation and provides very high bandwidth due to overall increase in the thickness of the microstrip patch antenna.
- This scheme also provides choices between two different dielectric media, one for the patch and one for the feed line to optimize the individual performances.
- Matching can be achieved by controlling the length of the feed line and the width-to-line ratio of the patch.
- The major disadvantage of this feed scheme is that it is difficult to fabricate because of the two dielectric layers which need proper alignment.
- Also, there is an increase in the overall thickness of the antenna.



Advantages

- Low fabrication cost, hence can be manufactured in large
- quantities.
- Easily integrated with microwave integrated circuits (MICs).
- Capable of dual and triple frequency operations.
- Supports both, linear as well as circular polarization.
- Low cost , Less size , Low Mass .
- Mechanically robust when mounted on rigid surfaces.
- High Performance
- Light weight and low volume.

Disadvantages

- Narrow bandwidth associated with tolerence problem
- Lower Gain(Nearly 6db) .
- Large ohmic losses in feed structure of arrays.
- Excitation of surface waves .
- Most microstrip antennas radiate into half-space .
- Relatively low efficiency (due to dielectric and conductor losses) .
- relatively high level of cross polarization radiation
- Spurious feed radiation (surface waves, strips, etc.)
- Inherently low impedance bandwidth.
- Low efficiency .
- Extraneous radiation from feeds and junctions .
- Low power handling capacity.

Remedies

- Low power and low gain can overcome by arrays configuration.
- Surface wave associated limitations such as poor efficiency, increased mutual coupling, reduced gain and radiation pattern can overcome.
- The band width can increase up to 60% by using some special techniques.
- In addition, as the substrate thickness increases, the radiation Q of the antenna decreases.
- Thus, impedance bandwidth increases with increasing substrate thickness.

Optimizing the Substrate Properties for Increased Bandwidth

The easiest way to increase the bandwidth of an MSA is to :

1) Print the antenna on a thicker substrate.

- However, thick substrates tend to trap surface wave modes , especially if the dielectric constant of the substrate is high .
- Finally if the substrate is very thick, radiating modes higher than the fundamental will be excited.

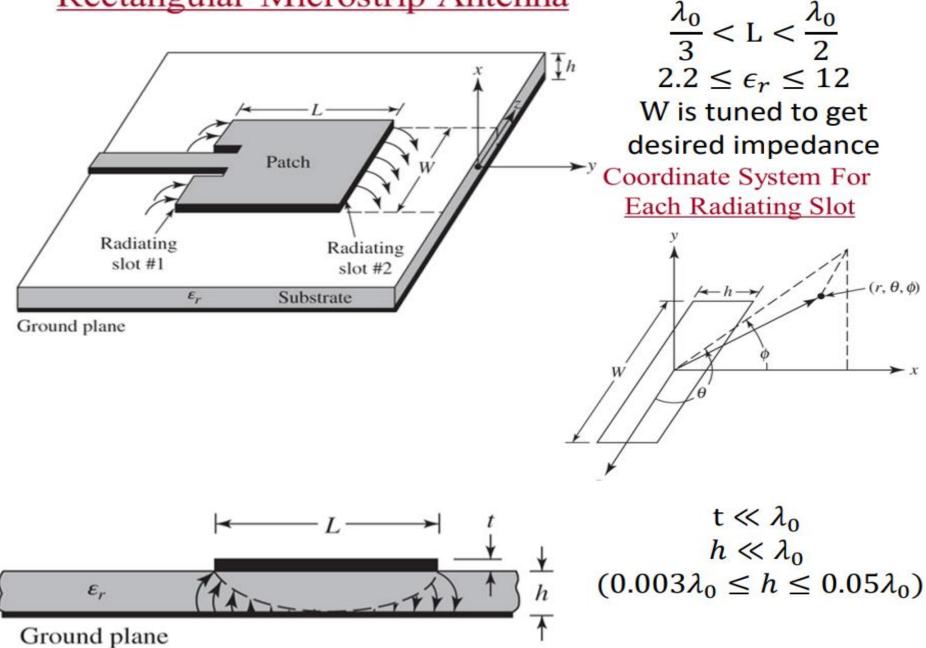
2) Decrease the dielectric constant of the substrate.

- However, this has detrimental effects on antenna size reduction since the resonant length of an MSA is shorter for higher substrate dielectric constant..
- In addition, the directivity of the MSA depends on the dielectric constant of the substrate.

3) Stack two patches on top of each other separated by a dielectric substrate or spacers.

• The application involved two identical circular patches stacked on top of each other. The lower patch was fed using a coaxial probe feed, and the top patch was electromagnetically coupled to the lower one .

Rectangular Microstrip Antenna



- Easy to fabricate
- Simple to match
- Low spurious radiation
- Narrow bandwidth
- Good for low h

 r, θ, ϕ

-x

Design of MSA patch length and width

Step 1: Calculation of the Width (W) -

$$W = \frac{c}{2f_o\sqrt{\frac{(\varepsilon_r+1)}{2}}}$$

Step 2: Calculation of the Effective Dielectric Constant. This is based on the height, dielectric constant of the dielectric and the calculated width of the patch antenna.

$$\varepsilon_{eff} = \frac{\varepsilon_r + 1}{2} + \frac{\varepsilon_r - 1}{2} \left[1 + 12 \frac{h}{W} \right]^{-\frac{1}{2}}$$

Step 3: Calculation of the Effective length $L_{eff} = \frac{c}{2f_o\sqrt{\varepsilon_{eff}}}$

Length of Patch (L) = $L_{eff} - 2\Delta L$ Length of Substrate $(L_g) = 6h + L$ Width of Substrate $(W_g) = 6h + W$ Step 4: Calculation of the length extension ΔL

$$\Delta L = 0.412h \frac{\left(\varepsilon_{eff} + 0.3\right)\left(\frac{W}{h} + 0.264\right)}{\left(\varepsilon_{eff} - 0.258\right)\left(\frac{W}{h} + 0.8\right)}$$

Step 5: Calculation of actual length of the patch

 $L = L_{eff} - 2\Delta L$

Where the following parameters are used

f₀ is the Resonance Frequency

W is the Width of the Patch

L is the Length of the Patch

h is the thickness

 ε_r is the relative Permittivity of the dielectric substrate

c is the Speed of light: 3 x 108

Rectangular Patch - Fields

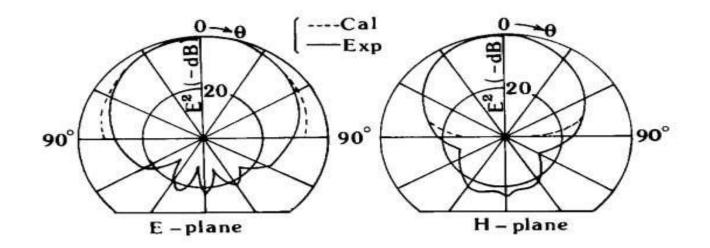
$$f(\theta,\phi) = \frac{\sin\left[\frac{kW}{2}\sin(\theta)\sin(\phi)\right]}{\frac{kW}{2}\sin(\theta)\sin(\phi)}\cos\left(\frac{kL}{2}\sin(\theta)\cos(\phi)\right)$$

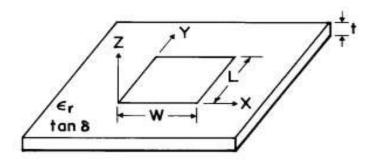
$$F_E(\theta) = \cos\left(\frac{kL}{2}\sin(\theta)\right), \qquad \phi = 0^\circ$$

$$F_{H}(\theta) = \cos(\theta) \frac{\sin\left(\frac{kW}{2}\sin(\theta)\right)}{\frac{kW}{2}\sin(\theta)}, \qquad \phi = 90^{\circ}$$

An approximate expression of the bandwidth for VSWR ≤ 2 , $|\Gamma| \leq \frac{1}{3}$, BW = 3.771 $\left[\frac{\epsilon_r - 1}{(\epsilon_r)^2}\right] \frac{h}{\lambda_0} \left(\frac{W}{L}\right)$

Radiation patterns of a rectangular microstrip patch antenna





Example

Design a rectangular microstrip antenna using a substrate (RT/duroid 5880) with dielectric constant of 2.2, h = 0.1588 cm (0.0625 inches) so as to resonate at 10 GHz.

Solution: Using (14-6), the width W of the patch is

$$W = \frac{30}{2(10)} \sqrt{\frac{2}{2.2+1}} = 1.186 \text{ cm} (0.467 \text{ in})$$

The effective dielectric constant of the patch is found using (14-1), or

$$\epsilon_{\text{reff}} = \frac{2.2+1}{2} + \frac{2.2-1}{2} \left(1 + 12 \frac{0.1588}{1.186}\right)^{-1/2} = 1.972$$

The extended incremental length of the patch ΔL is, using (14-2)

$$\Delta L = 0.1588(0.412) \frac{(1.972 + 0.3) \left(\frac{1.186}{0.1588} + 0.264\right)}{(1.972 - 0.258) \left(\frac{1.186}{0.1588} + 0.8\right)}$$

= 0.081 cm (0.032 in)

The actual length L of the patch is found using (14-3), or

$$L = \frac{\lambda}{2} - 2\Delta L = \frac{30}{2(10)\sqrt{1.972}} - 2(0.081) = 0.906 \text{ cm} \ (0.357 \text{ in})$$

Finally the effective length is

$$L_e = L + 2\Delta L = \frac{\lambda}{2} = 1.068 \text{ cm} (0.421 \text{ in})$$

An experimental rectangular patch based on this design was built and tested. It is probe fed from underneath by a coaxial line and is shown in Figure 14.8(a). Its principal E- and H-plane patterns are displayed in Figure 14.19(a,b).

Örnek: Design microstrip antenna fo=1.85GHz

$$W = \frac{c}{2f_o\sqrt{\frac{(\varepsilon_r+1)}{2}}} \qquad \varepsilon_{reff} = \frac{\varepsilon_r+1}{2} + \frac{\varepsilon_r-1}{2} \left[1+12\frac{h}{W}\right]^{-\frac{1}{2}} \qquad \Delta L = 0.412h \frac{\left(\varepsilon_{reff}+0.3\right)\left(\frac{W}{h}+0.264\right)}{\left(\varepsilon_{reff}-0.258\right)\left(\frac{W}{h}+0.8\right)}$$

$$c = 3 \times 10^{\circ}8 \text{ m/sec}$$

$$\varepsilon_r = 11.9$$

$$h = 1.59 \text{ mm}$$

$$W = 31.9 \text{ mm}$$

$$Therefore,$$

$$W = 31.9 \text{ mm}$$

$$Therefore,$$

$$W = 31.9 \text{ mm}$$

$$W = 31.9$$

The effective length of the patch L_{eff} now becomes:

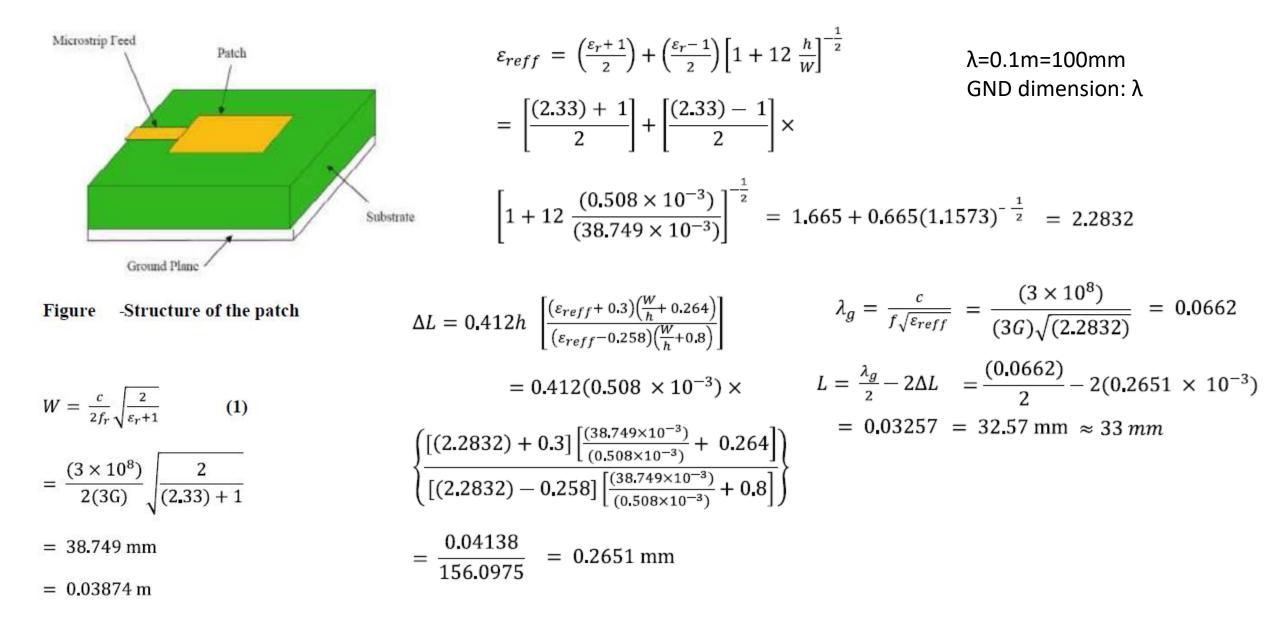
$$L_{eff} = L + 2\Delta L$$

For a given resonance frequency f_o , the effective length is given by as:

$$L_{\rm eff} = \frac{c}{2f_o\sqrt{\varepsilon_{\rm reff}}}$$

 $\mathcal{E}_{reff} = 10.7611$ therefore, the value of L_{eff} is 24.7 mm & value of L will be 23.36 mm.

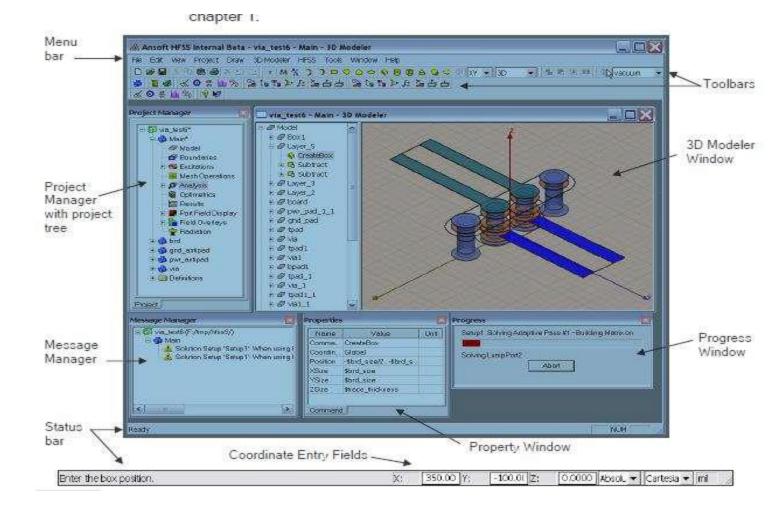
Örnek: Design microstrip antenna fo=3GHz



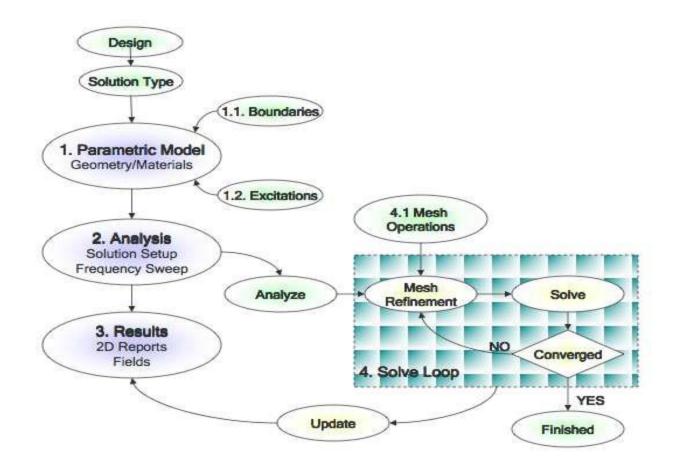


Designing the Microstrip patch

- HFSS stands for high frequency structure simulator
- ANSYS HFSS software is the industry standard for simulating 3-D full wave electromagnetic fields.



Designing the Microstrip patch



Design specification of rectangular patch antenna

3D model

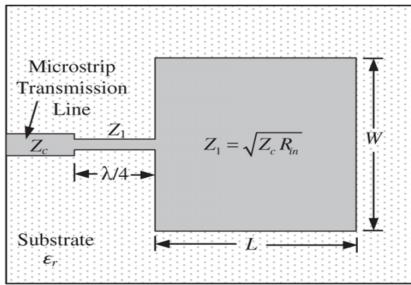
- Ground: Wg,Lg
- Substrate: Wg, Lg, h, ε_r
- Microstrip line(feed): Wf, Lf
- Radiated Patch: W, L
- Lumped Port: 1mm
- Radiation measure wall: R

Tüm uzunluklar dalga boyunun katsayı çarpımı ile ifade edilir.

Assigning boundary: Perfect E

Assigning excitation: Lumped Port, Radiation

Matching Techniques



 $\lambda/4$ impedance transformer

Analysis of patch antenna

Analysis setup

- solution freq
- max number of passes
- max Delta S per pass

Freq sweep

- starting freq
- attenuating freq
- number of counting

Analyze

Örnek: Design microstrip antenna fo=2.4GHz, εr=4.4, h=1.5mm

 $\lambda = \frac{c}{f} = \frac{3 \times 10^8}{2.4 \times 10^9} = 0.125 \text{m} = 125 \text{mm}$

$$W = \frac{\lambda/2}{\sqrt[2]{\frac{\varepsilon_r + 1}{2}}} = 0.038 \text{m} = 38 \text{mm}$$

$$\varepsilon_{eff} = \frac{\varepsilon_r + 1}{2} + \frac{\varepsilon_r - 1}{2} \left[1 + \frac{12h}{W} \right]^{-\frac{1}{2}} = 4.24$$

$$L_{eff} = \frac{\lambda/2}{\sqrt[2]{\varepsilon_{eff}}} = 30.34$$
mm

$$\Delta L = 0.412h \frac{(\varepsilon_{eff} + 0.3)(\frac{W}{h} + 0.264)}{(\varepsilon_{eff} - 0.258)(\frac{W}{h} + 0.8)} = 0.69 \text{mm}$$

Length of Ground Plane, $L_g = \lambda$

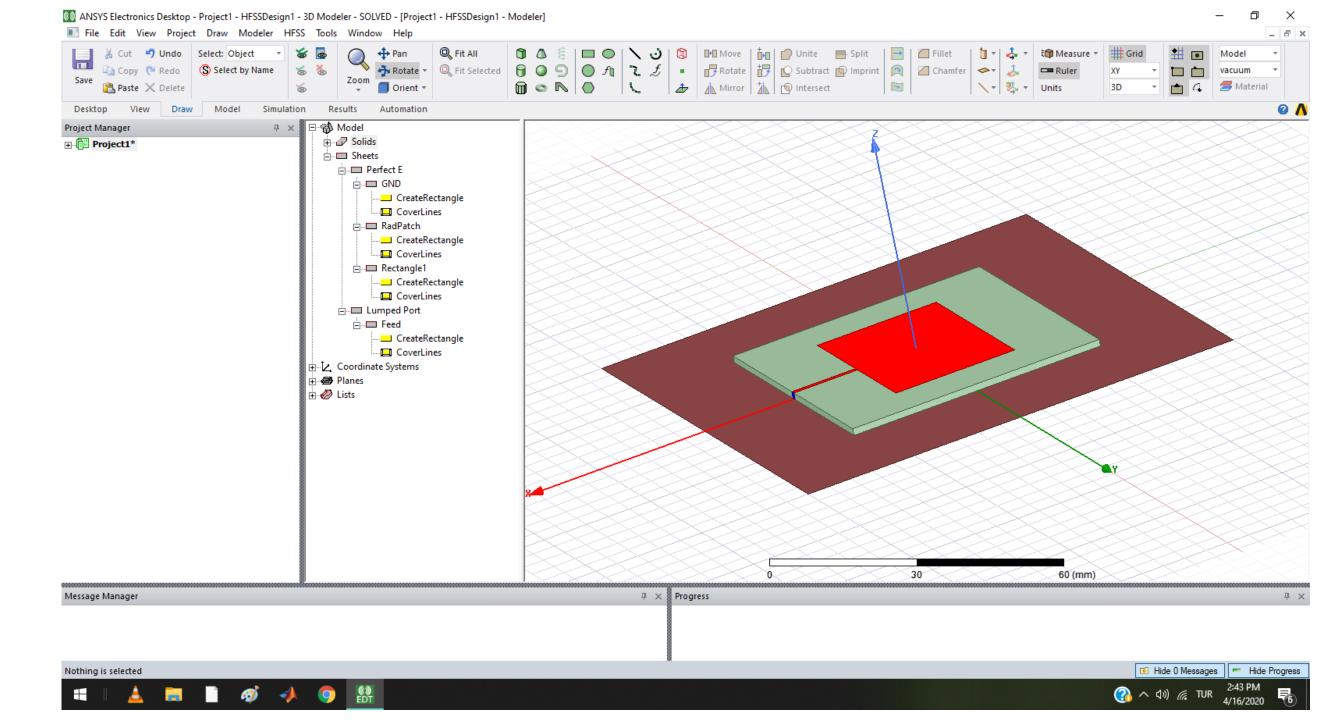
Width of Ground Plane, $W_q = \lambda$

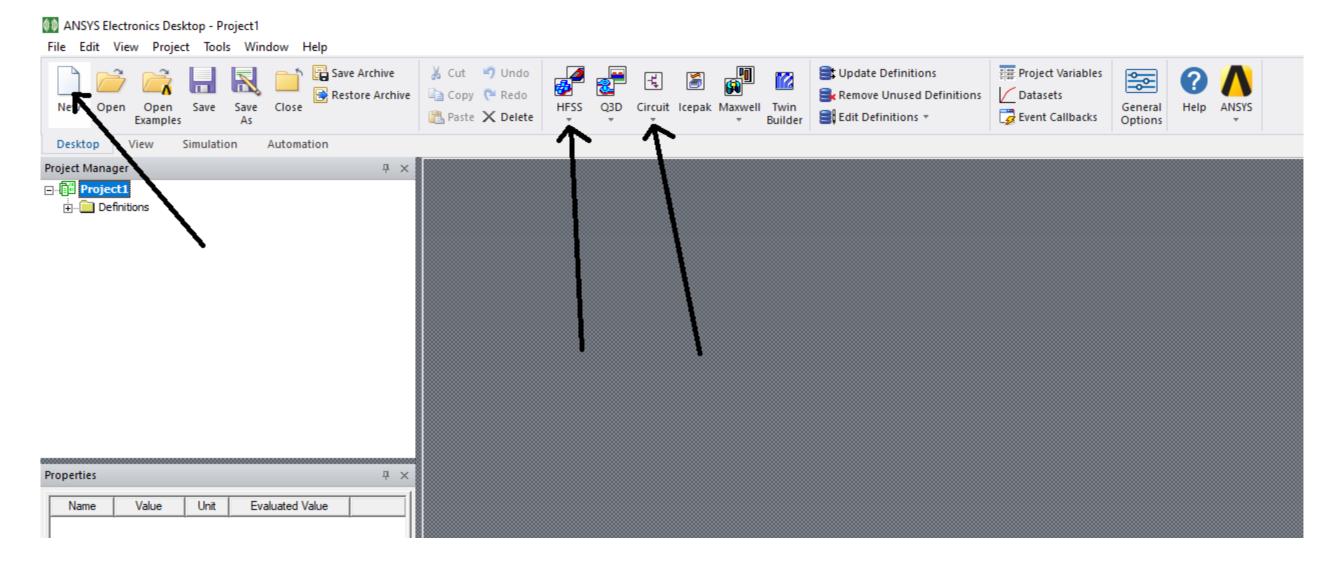
 $L = L_{eff} - 2\Delta L = 29mm$

$$\lambda_g = \frac{\lambda}{\sqrt[2]{\mathcal{E}_{eff}}} = 60 \text{mm}$$

Length of Substrate, L_s =L+ λ g/2=59mmm

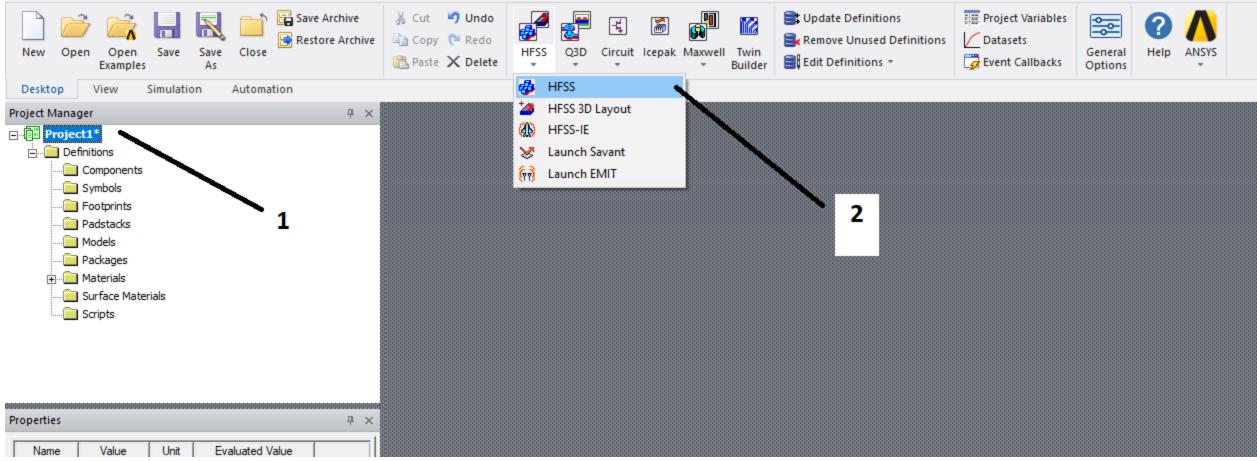
Width of Substrate, W_s =W+ λ g/4=68mm

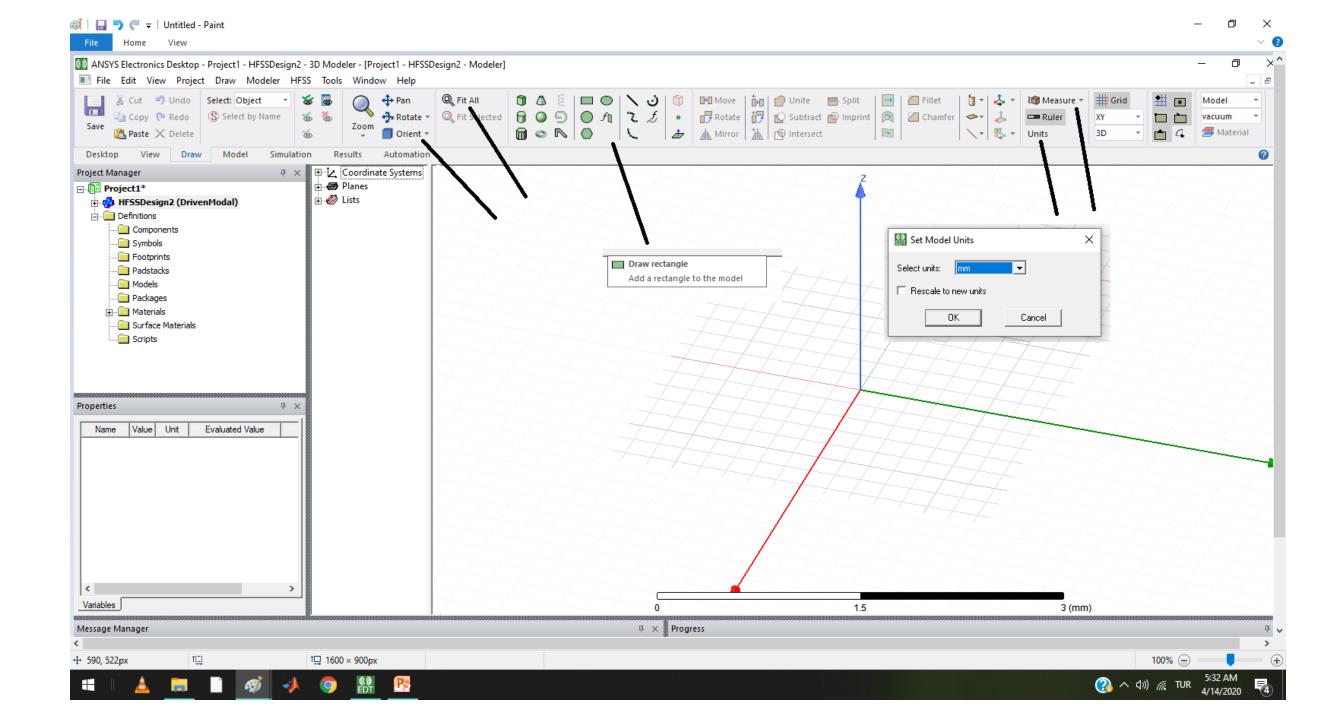




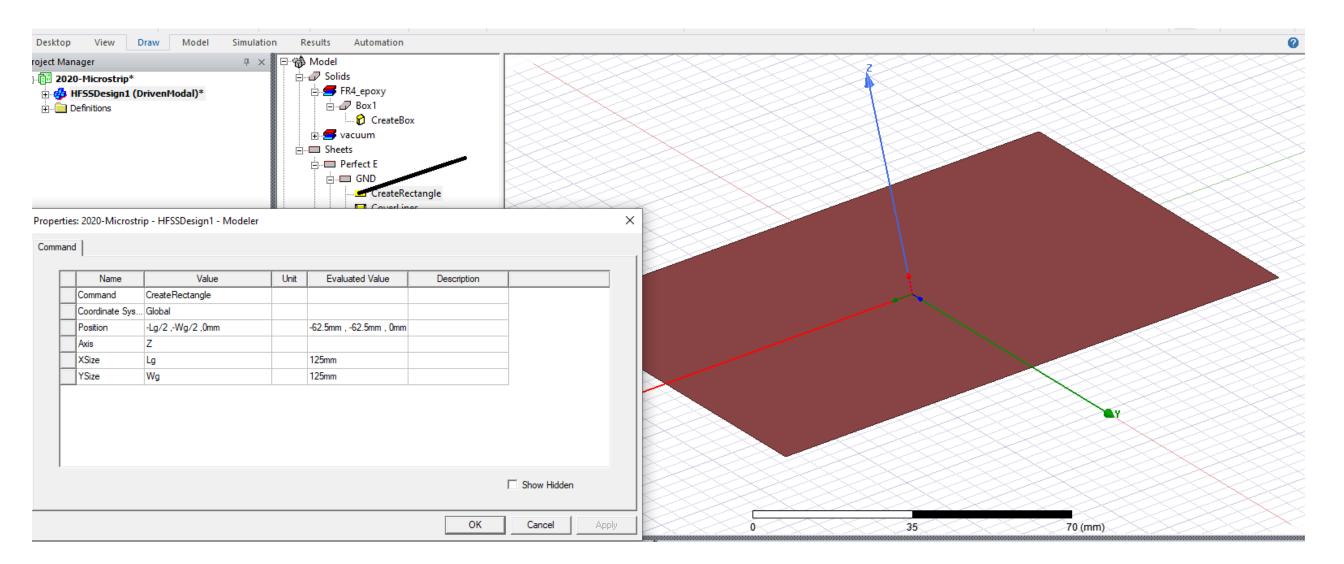


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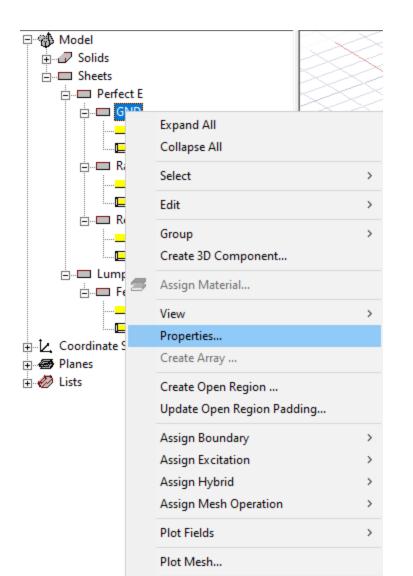




GND

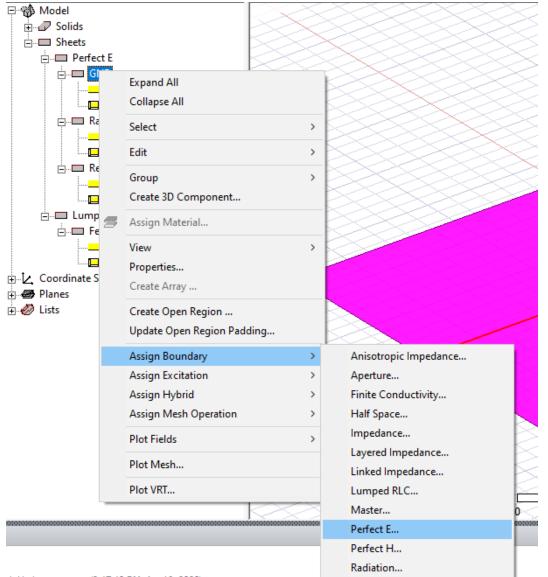


GND – Properties: Name, Color

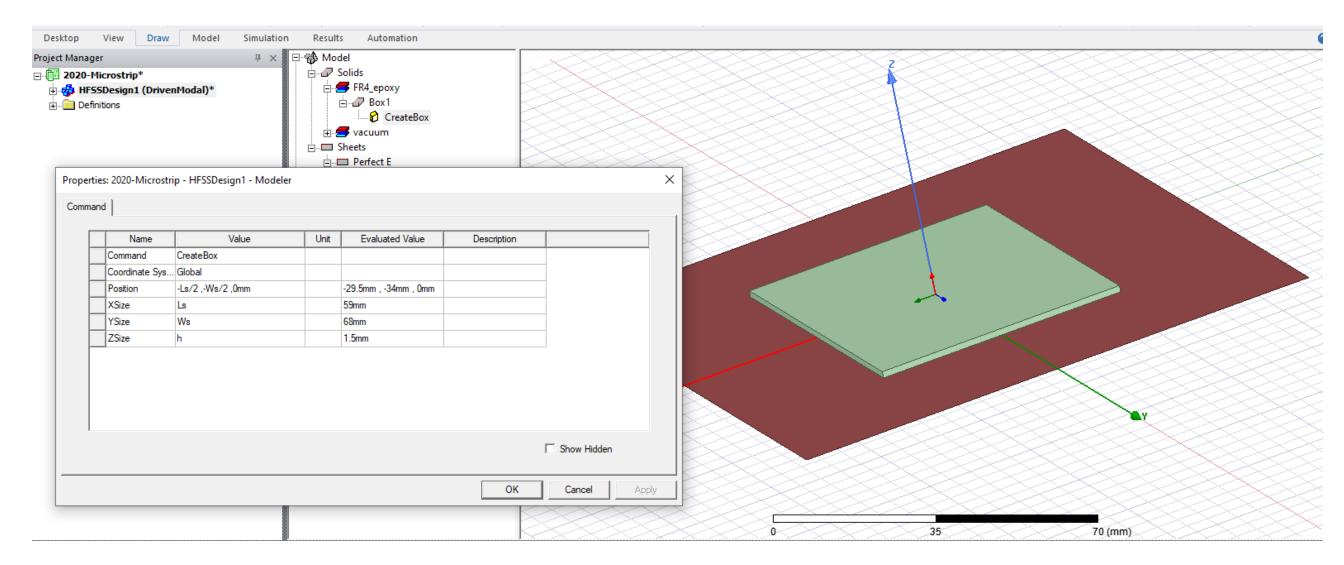


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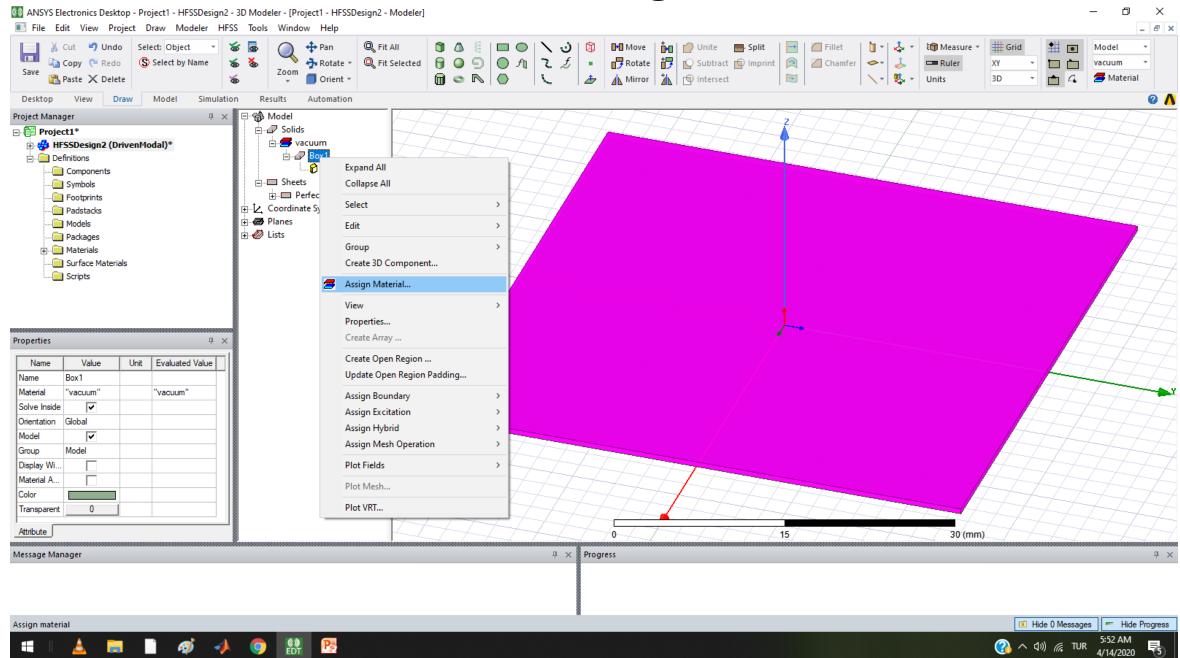
GND – Properties: Assign Boundary - Perfect E



Substrate



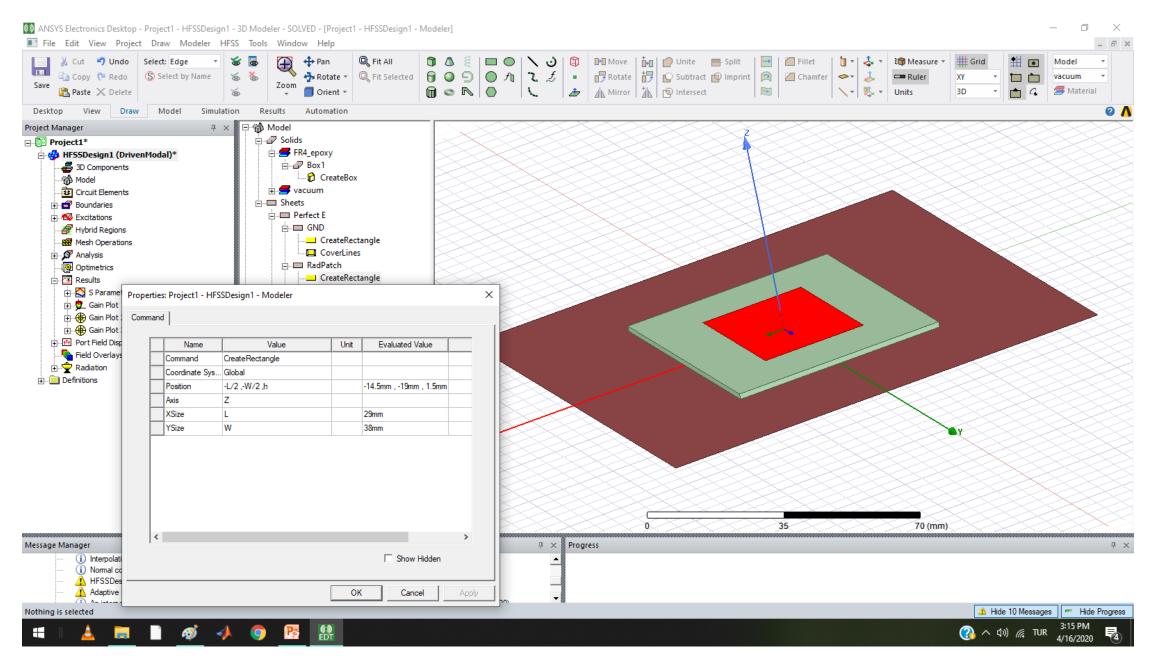
Substrate – Assign material



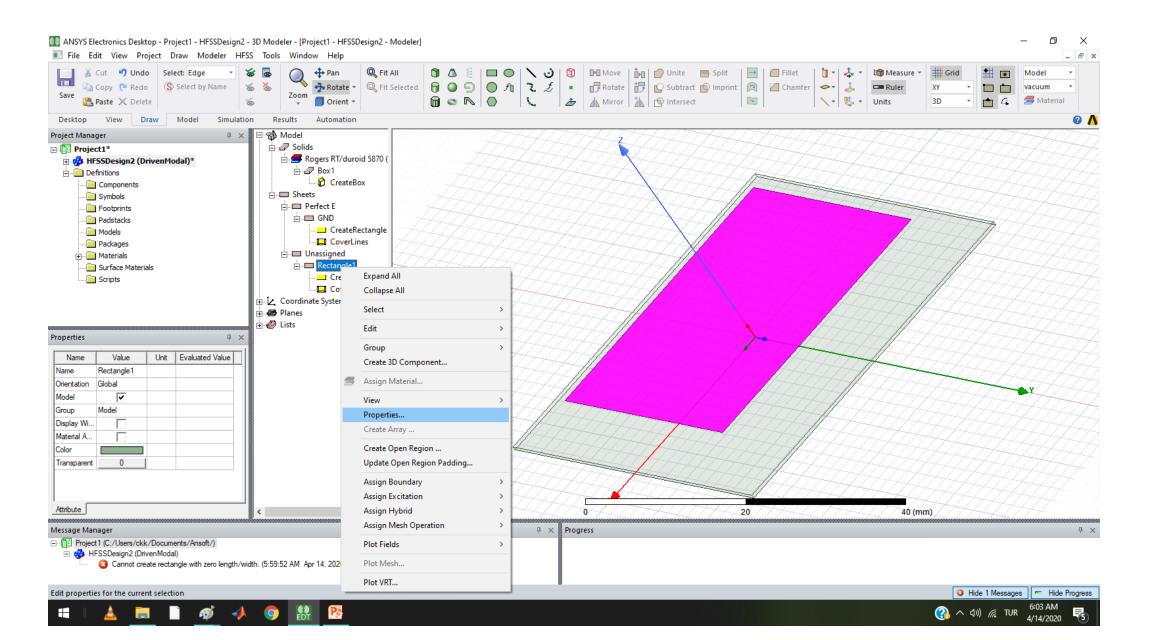
Substrate - Material

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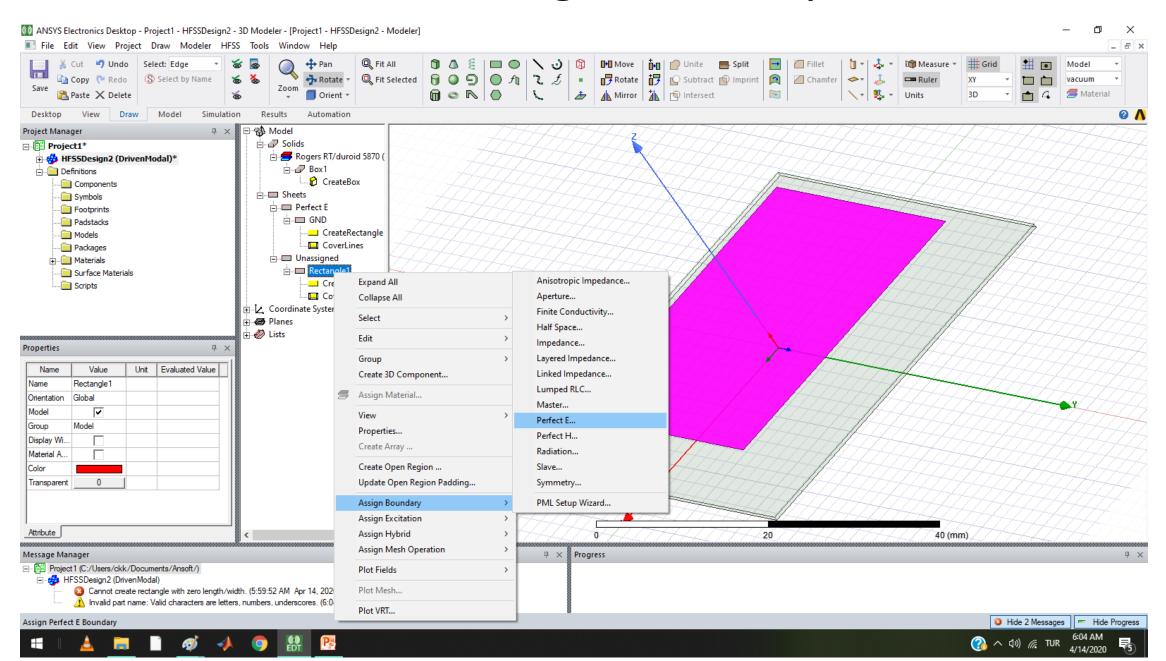
Radiated Part



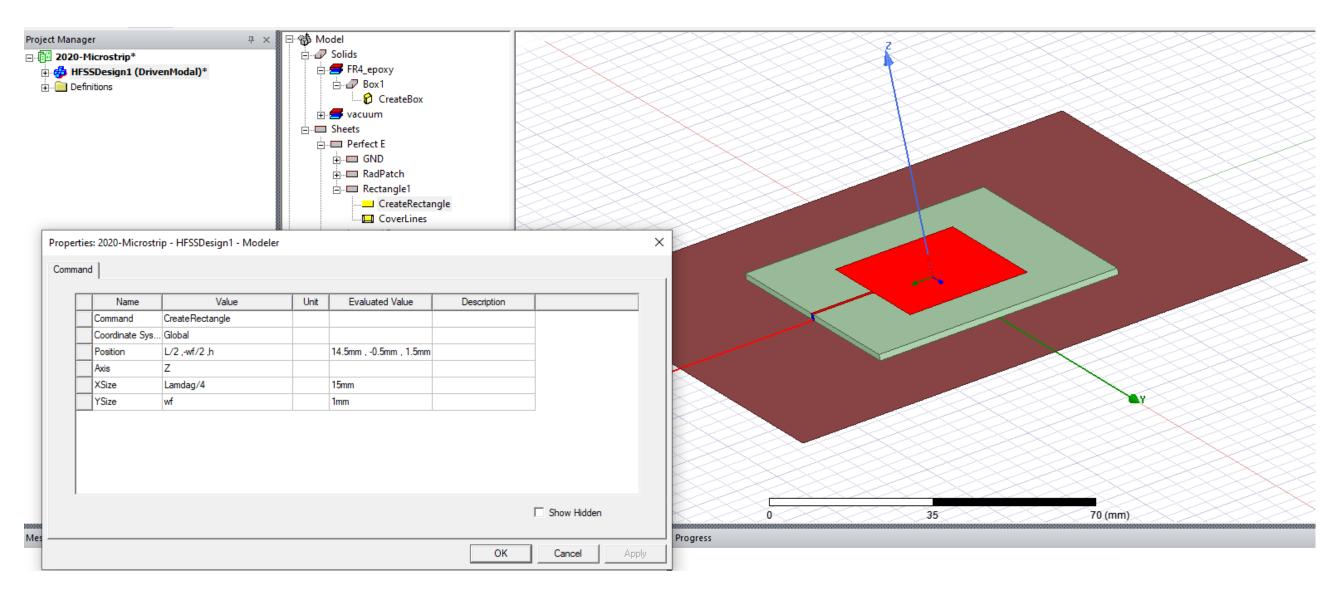
Radiated Part – Properties (Name, Color)



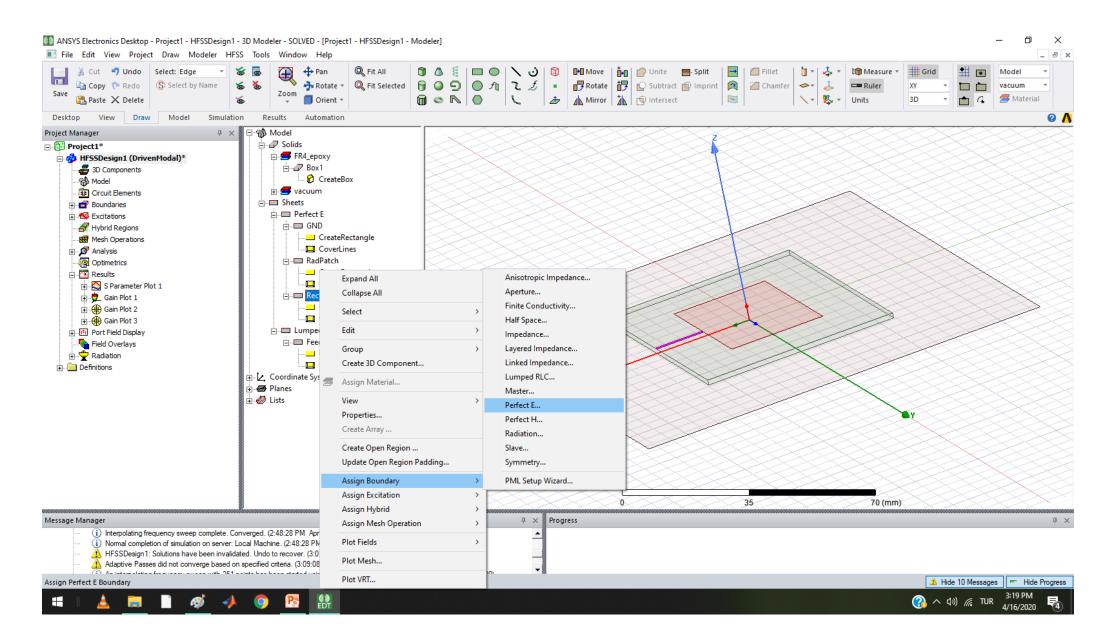
Radiated Part – Assign Boundary- Perfect E



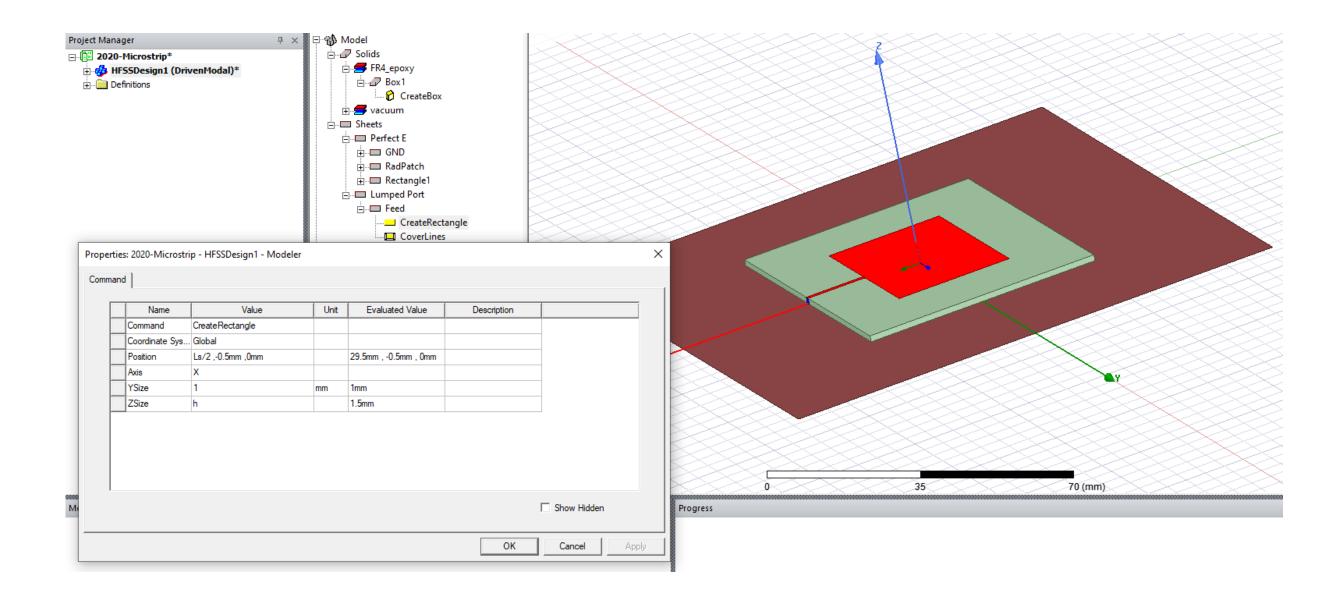
Feed Line



Feed Line– Assign Boundary- Perfect E



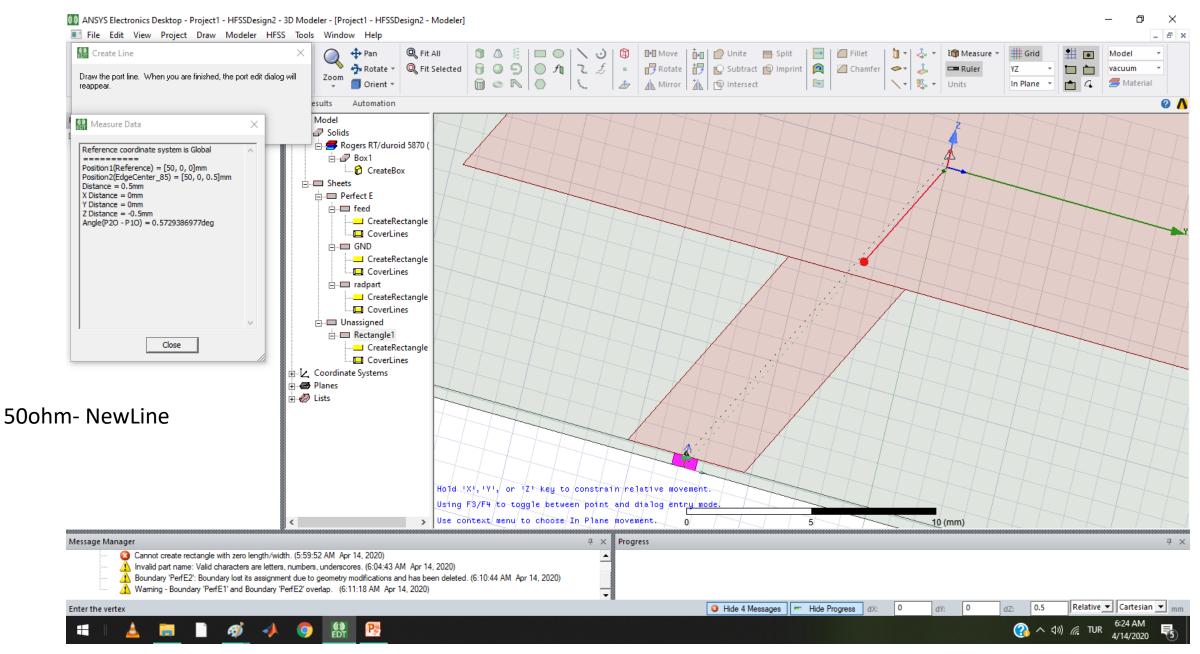
Feed – Lumped Port



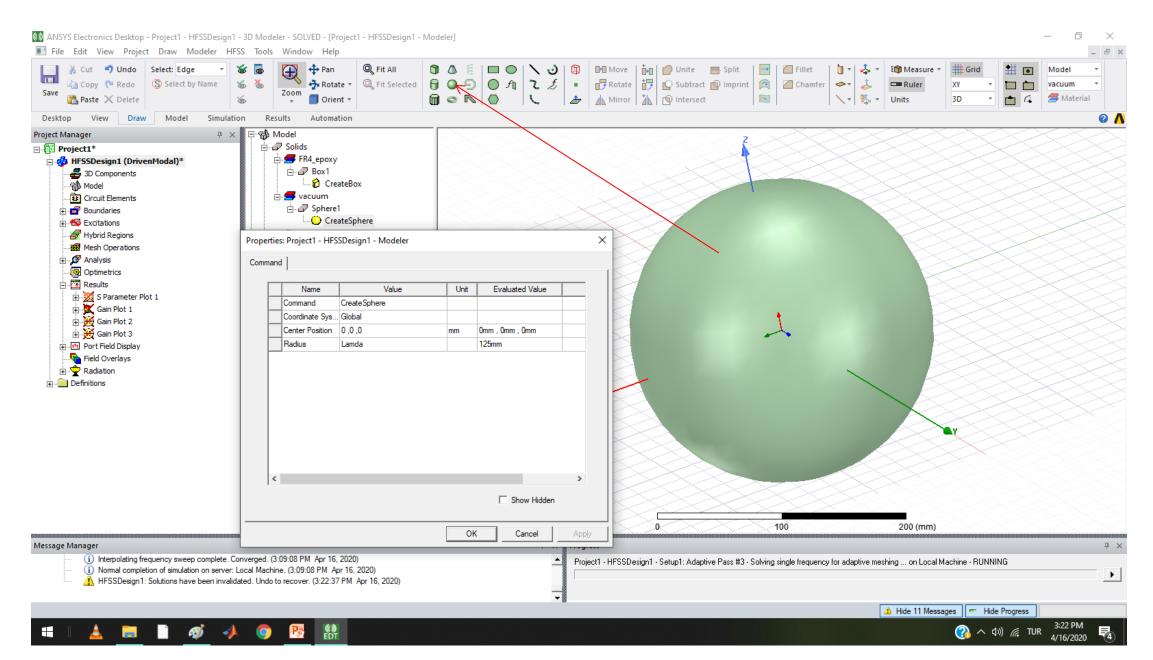
Feed – Lumped Port

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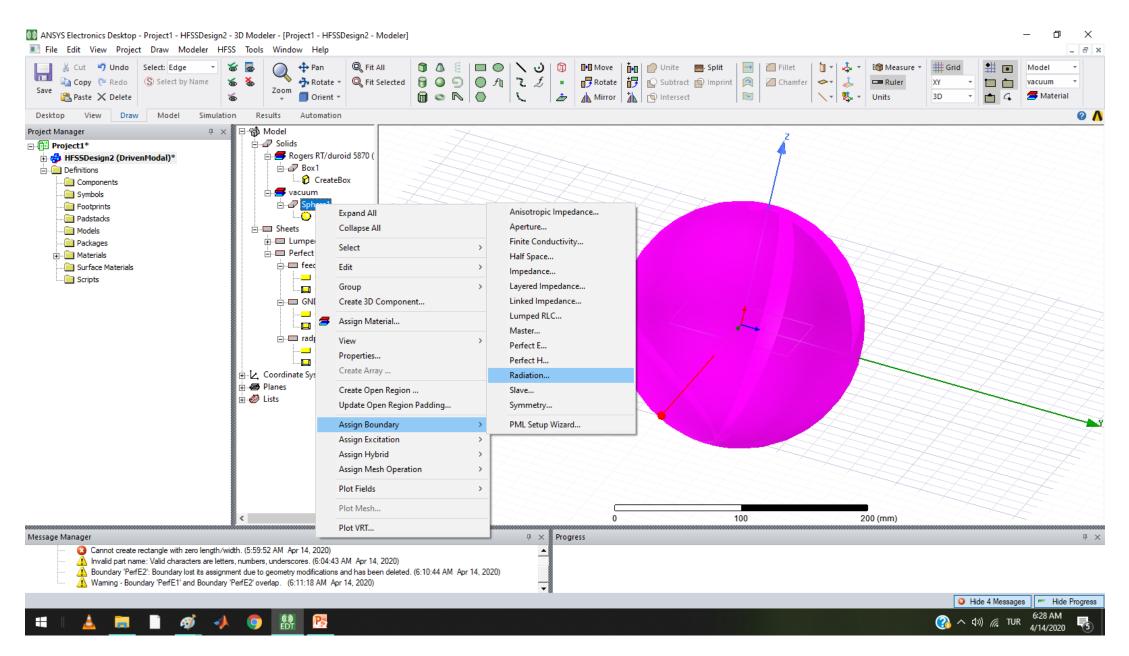
Feed – Lumped Port



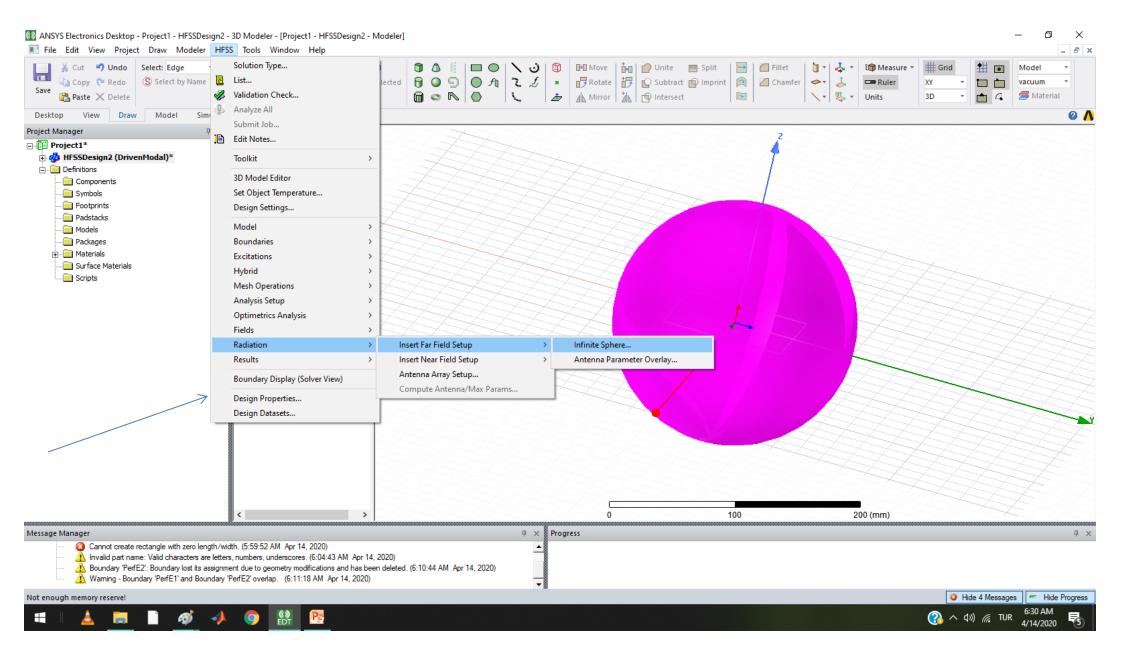
Radiation



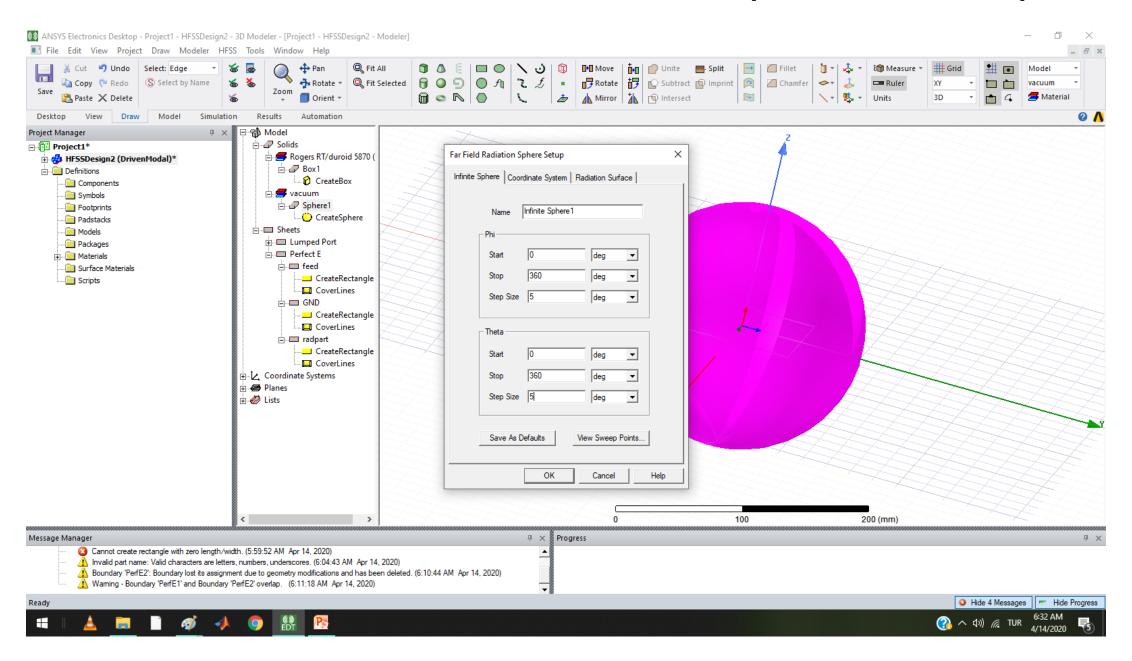
Assign Boundary - Radiation



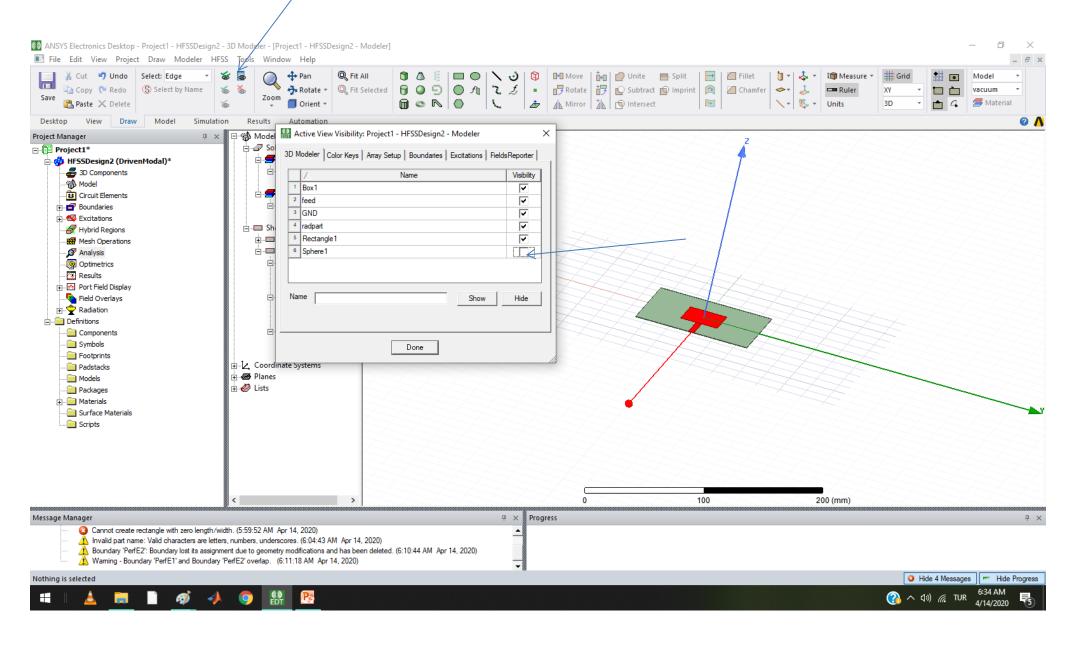
HFSS-Radiation-Insert Far Field Setup – Infinite Sphere



HFSS-Radiation-Insert Far Field Setup – Infinite Sphere



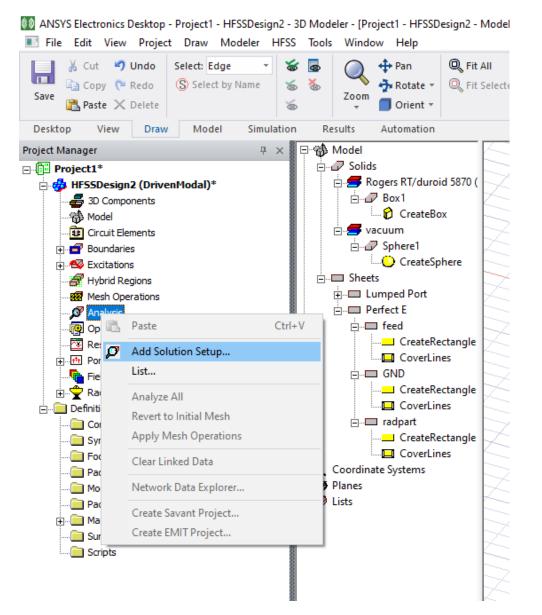
Radiation-No view



Parametrik değerlerin değiştirilmesi

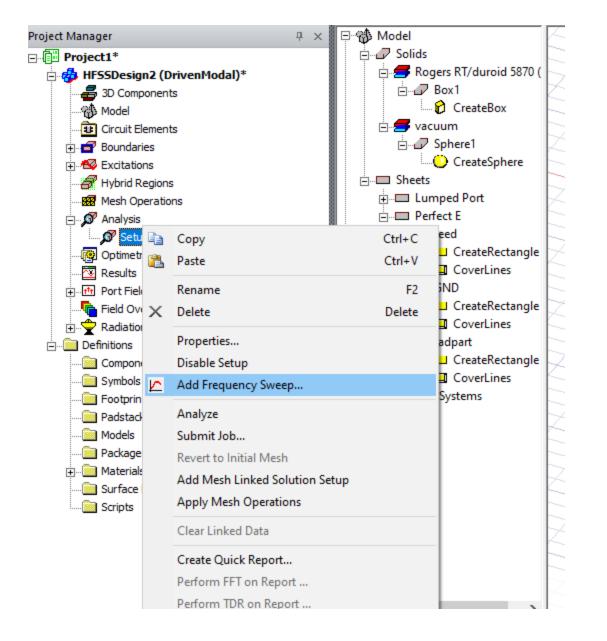
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Test: Return Loss, S11

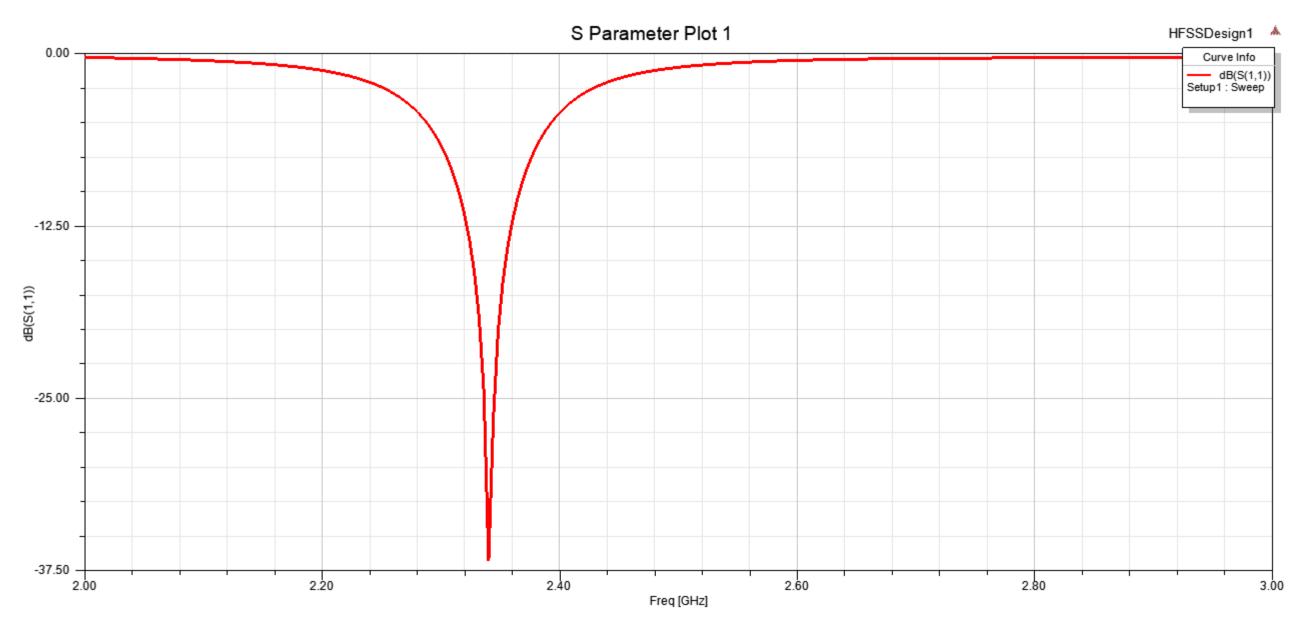
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Report: Project1 - HFSSDesign2 - New Report - New Trace(s)

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Test S11

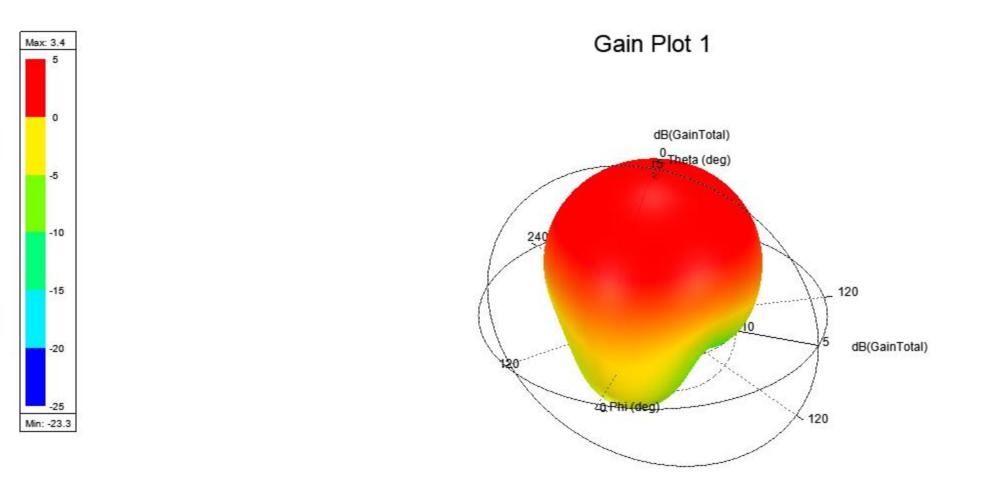


Test – Pattern

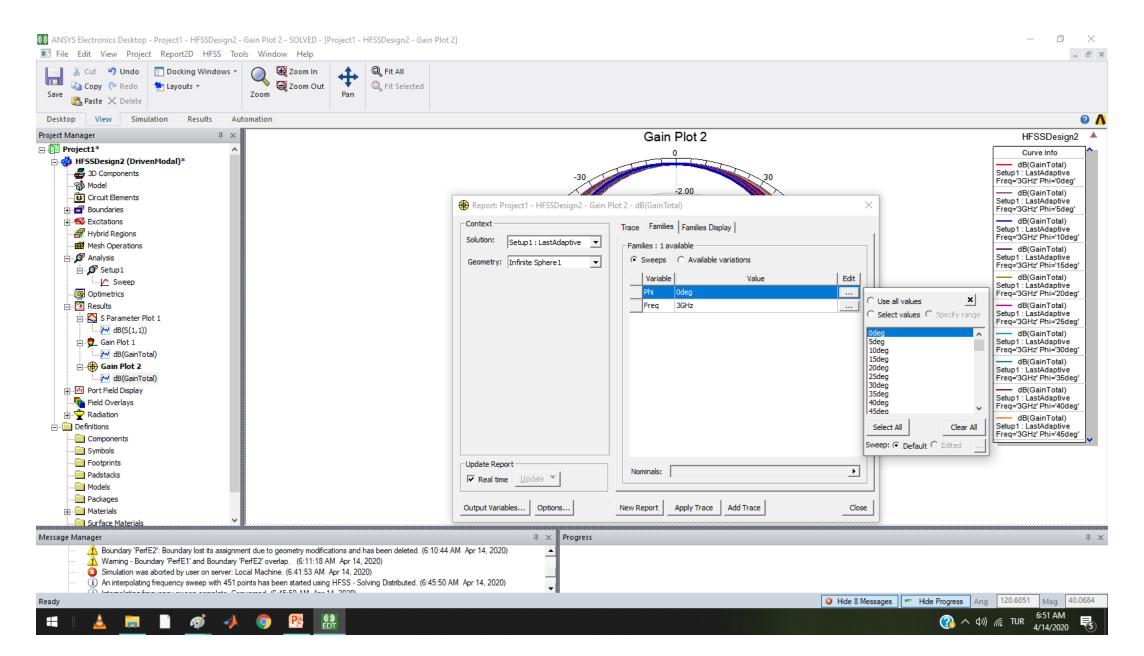
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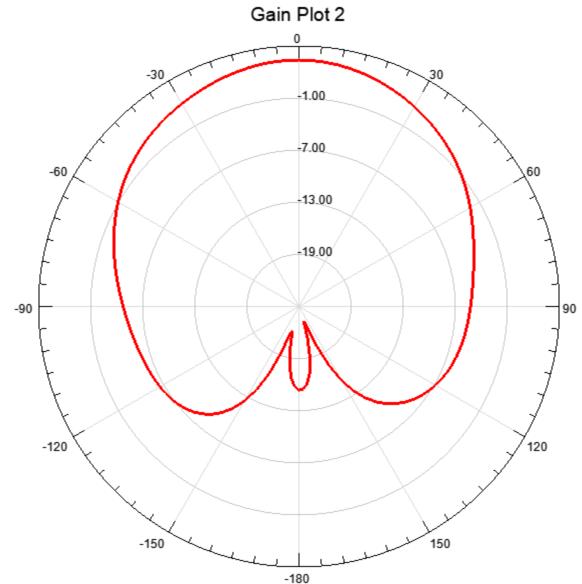
Test – Pattern

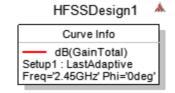


Test: E-Pattern

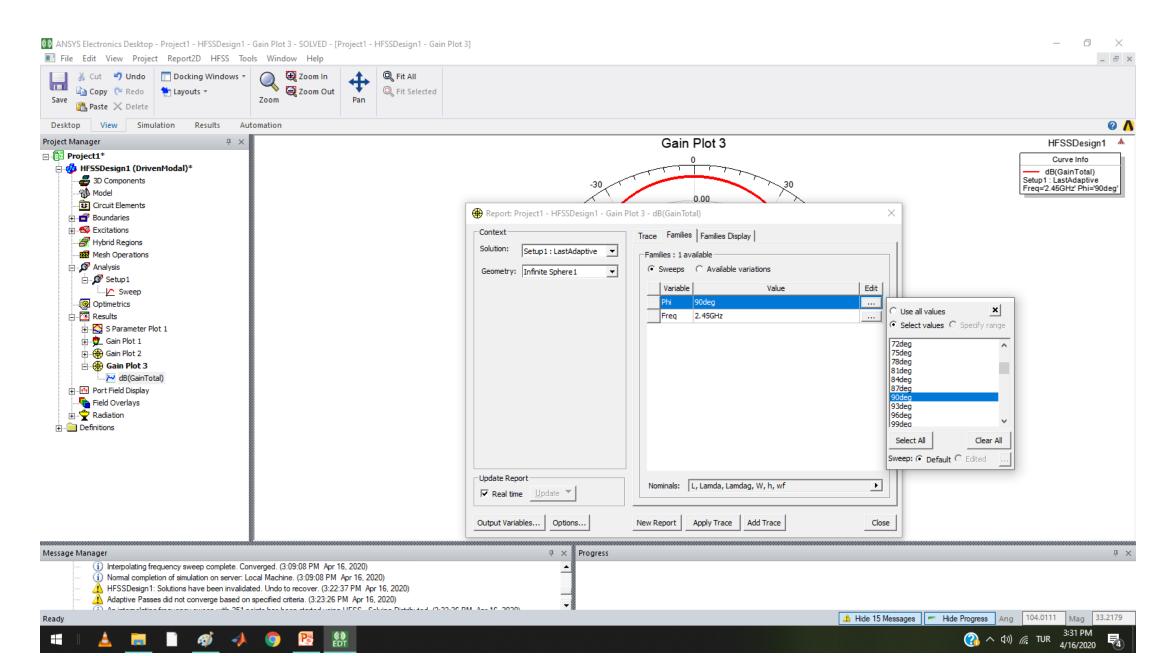


Test: E-Pattern

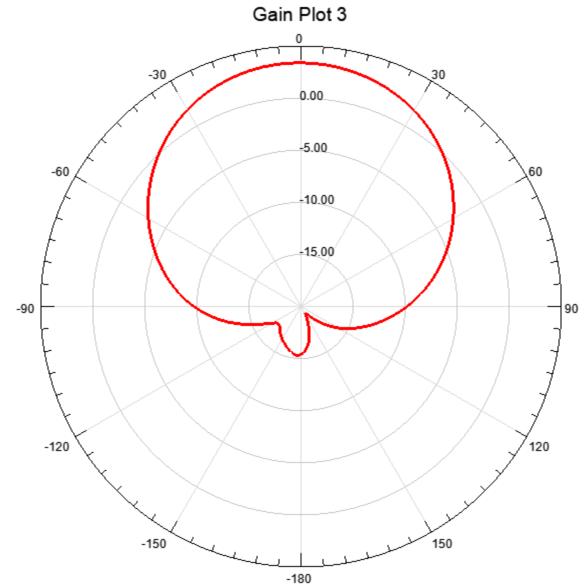


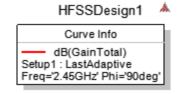


Test: H-Pattern



Test: H-Pattern



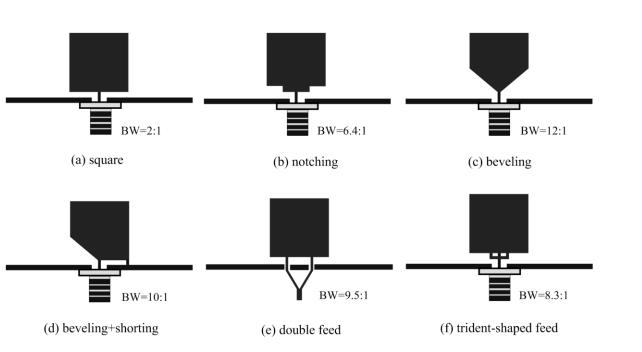


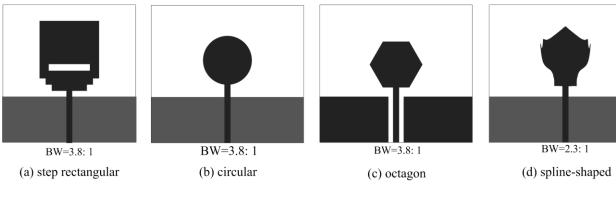
SQUARE PLANAR MONOPOLE ANTENNA

Square Planar Monopole Antenna

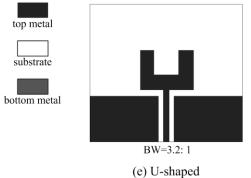
- 1991 yılında Honda tarafından düzlemsel bir disk tekel anteni incelendi.
- Japon televizyonları için bu anteni (90-770 MHz) geliştirdi.
- 1992'de tüm S, C, X ve Ku bantları için geri dönüş kaybı 10 dB'den fazla olan, yani 1:18 bant genişliği olduğunu bildirdi.
- Düzlemsel bir monopol, geleneksel bir monopolün tel elemanının bir düzlemsel eleman ile değiştirilmesiyle gerçekleştirilir.
- Kare olan düzlemsel eleman, bir toprak düzleminin üzerine yerleştirilir ve bir SMA konektörü kullanılarak beslenir.

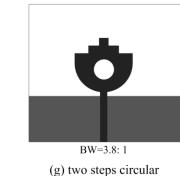
Monopole Antenna Types



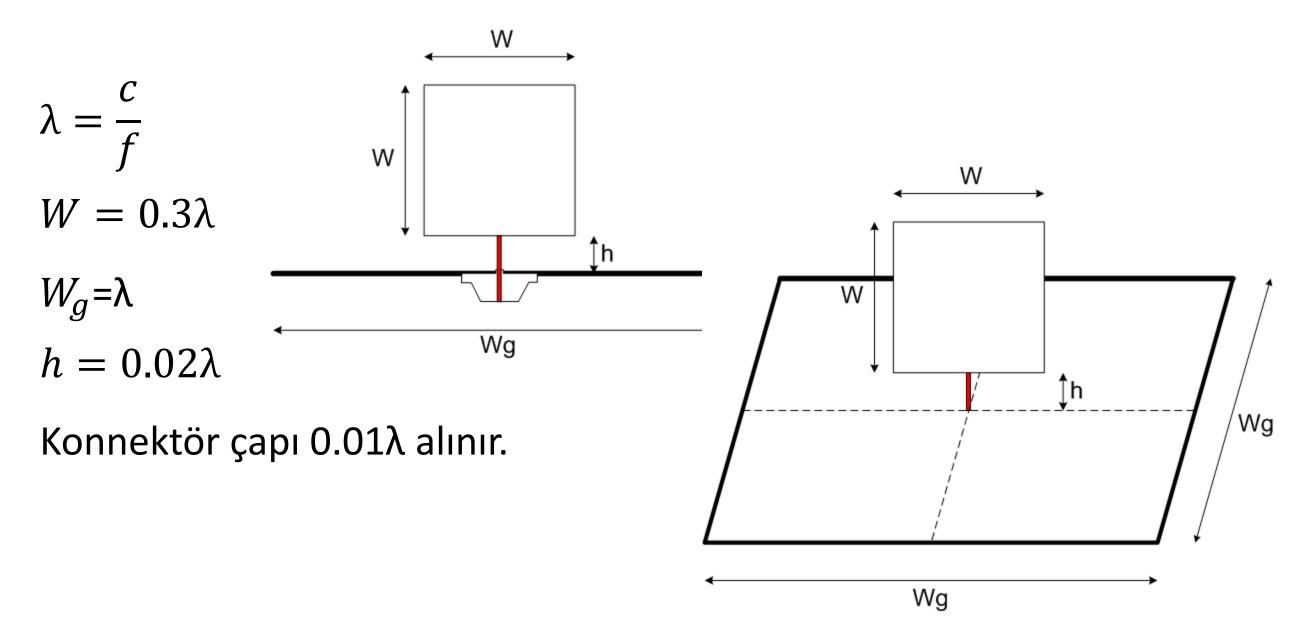


BW=3.2: 1 (f) Knight's helm

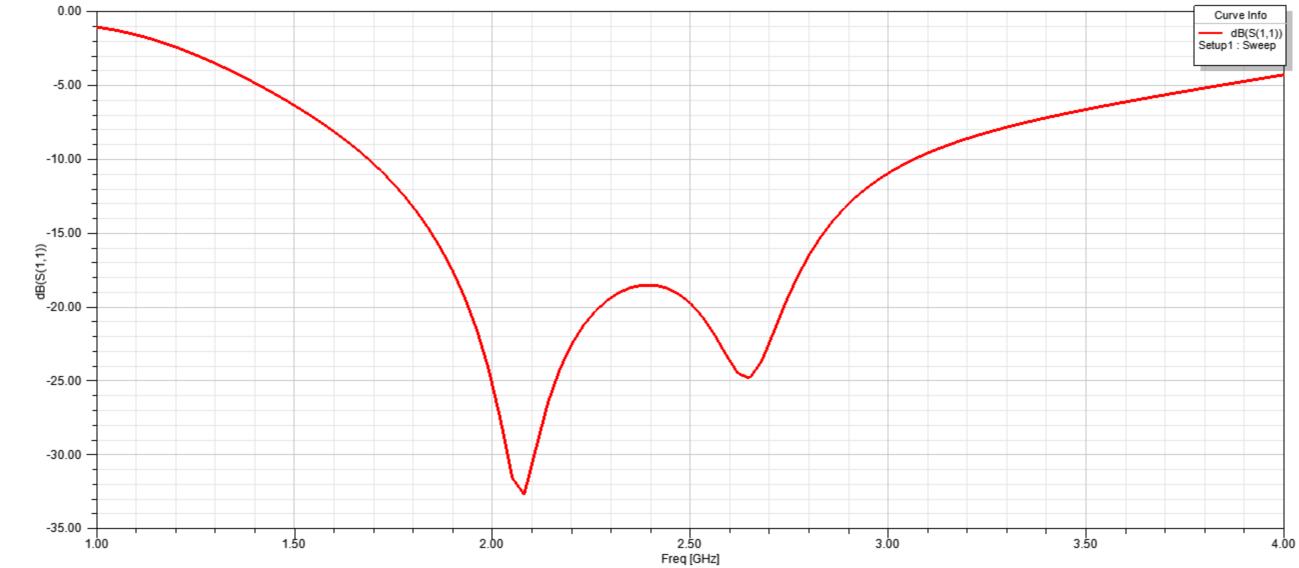




Square Planar Monopole Antenna

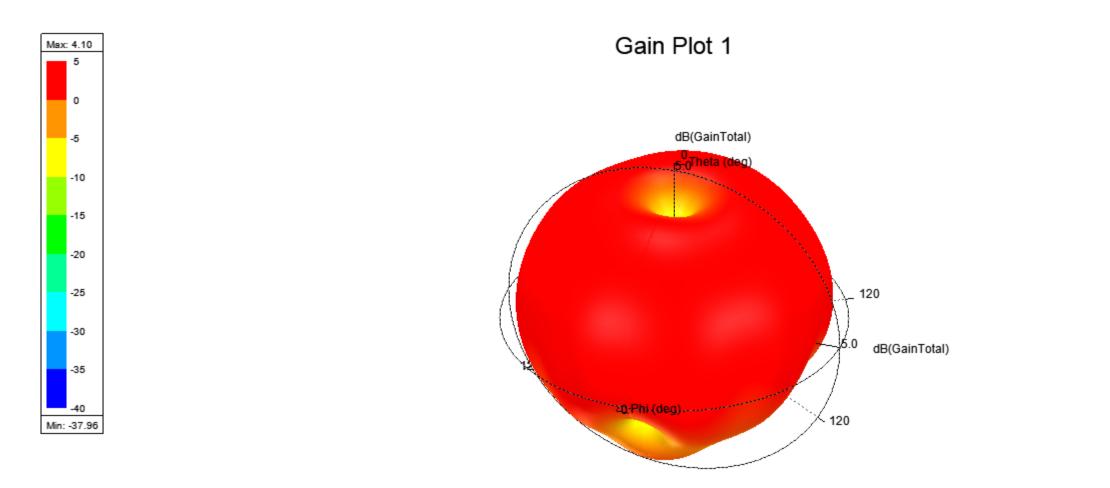


S Parameter Plot 1

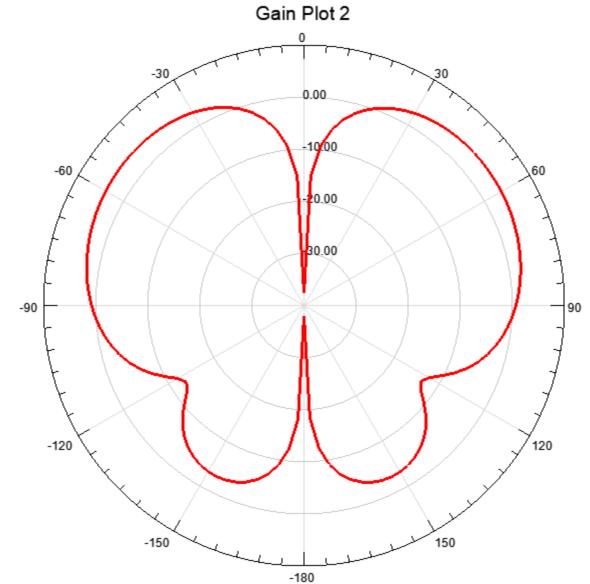


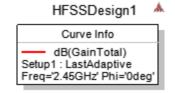
HFSSDesign1 🔺

Gain (Far Field report – 3D Polar Plot)

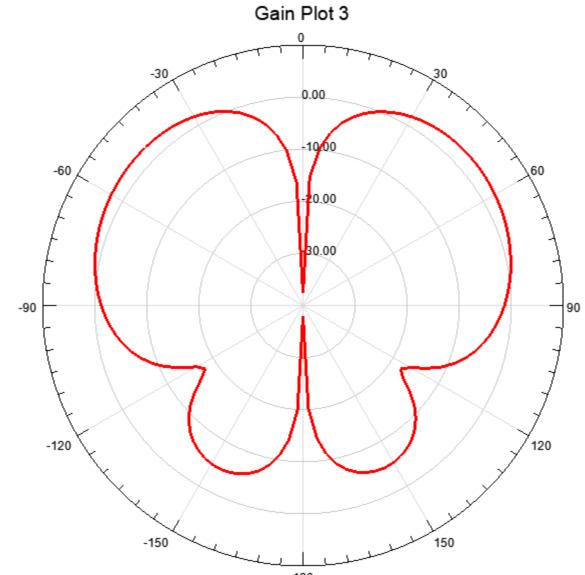


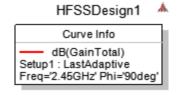
E-Pattern (90derece)





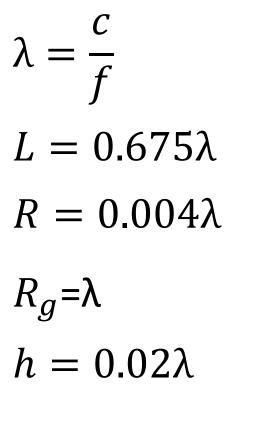
H-Pattern (0 derece)



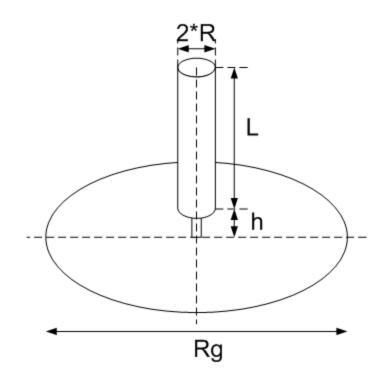


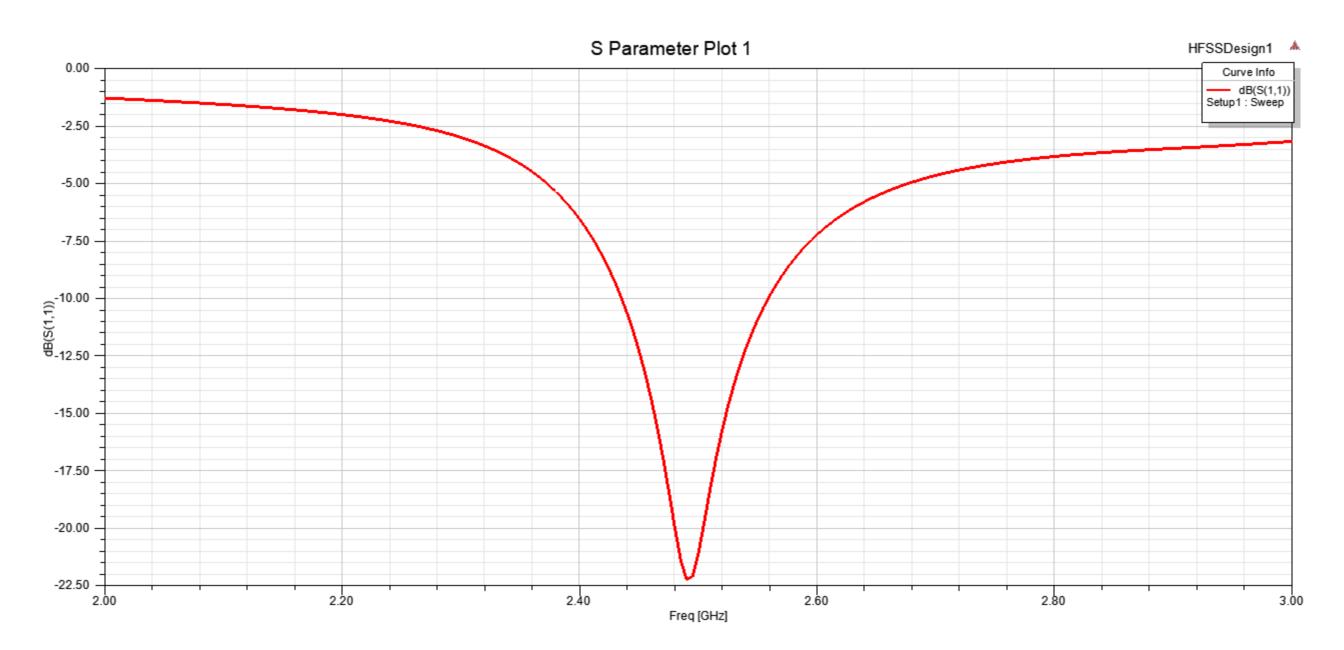
Dipole Antenna

Dipole Antenna Design

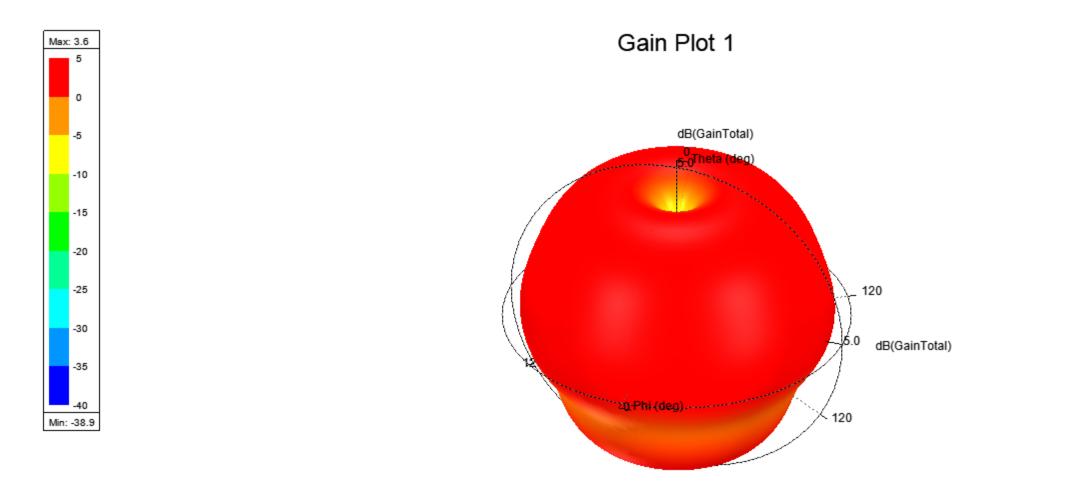


Konnektör çapı 0.01λ alınır.

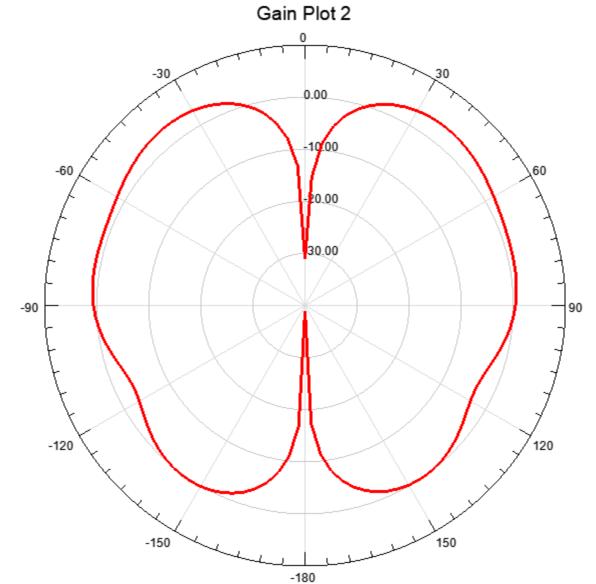


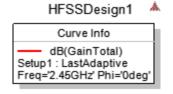


Gain (Far Field report – 3D Polar Plot)

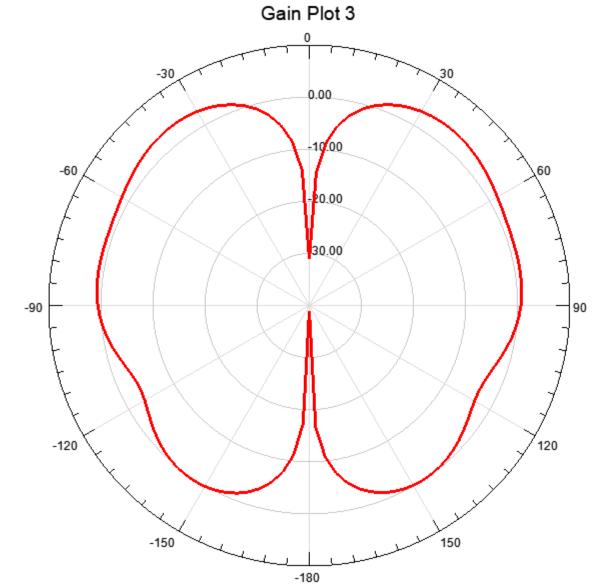


E-Pattern (90derece)

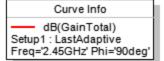




H-Pattern (Oderece)







Anten Parametreleri Ölçümü:

Işıma Paterni S11-Return Loss, VSWR Gain

Konnektör Tipleri







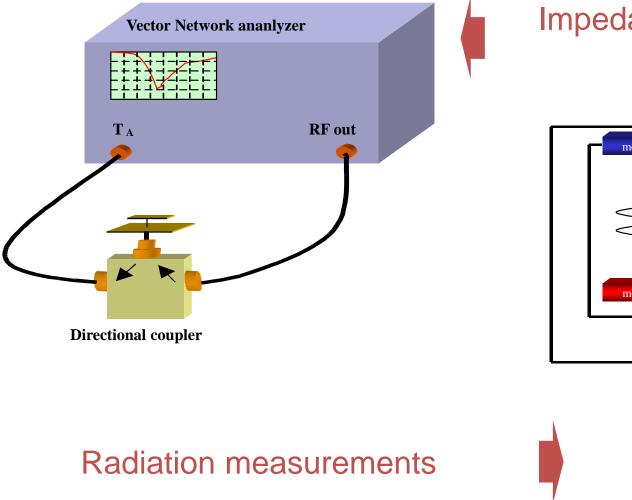


PCB Connectors

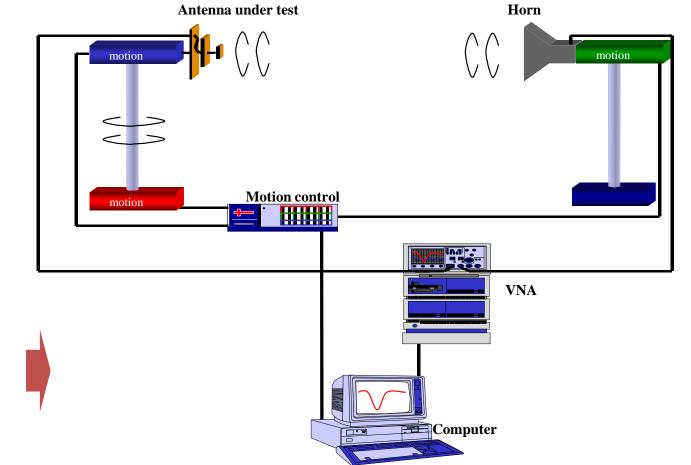




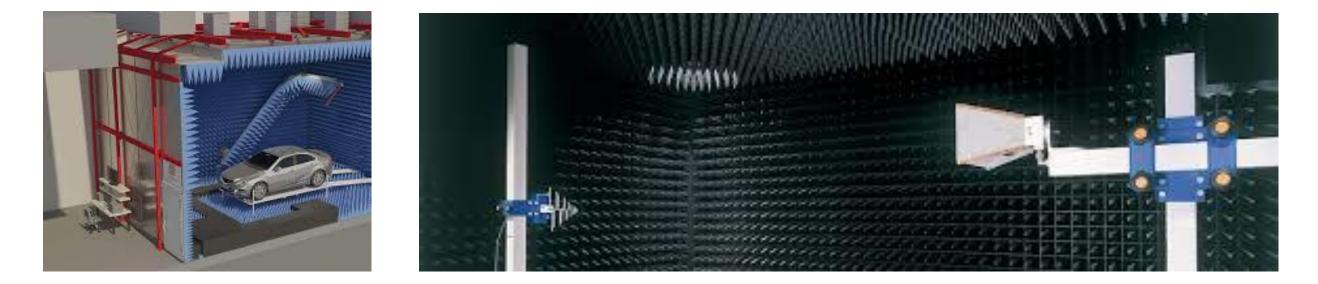
Measurement methods



Impedance matching measurements



Yansımasız Oda





Radome

- Bu nedenle, anten sistemini havanın bu olumsuz etkilerinden, dış erişim tehditlerinden korumak için radom kullanılır.
- Radom, anten üzerinde olumsuz etkiler yaratan toz, su, su buharı, rüzgar, böcekler, partiküller, güneş radyasyonu, vs.den anteni korur. 250 km/saat rüzgar hızına dayanabilmelidir.
- Radomun iç sıcaklığı -50 +60°C olması durumunda çalışabilmelidir. Isıtma yapılacaksa tamamen kuru havayla yapılmalıdır. Radom üzerine çok yağış düştüğünde antenin düşeydeki polarizasyonu kaybolur.
- Önemli olan kılıfta kullanılan malzemenin elektromanyetik dalgaların geçişine olabildiğince uygun olmasıdır.
- Bu yapının adı RAdar DOMe (yani radar-kubbe) kelimelerinden türetilmiştir.
- Bu koruyucu kaplama, elektromanyetik dalgaları olabildiğince az yansıtmalı, soğurmalı (absorbtion), kırmalı (diffraction) veya saçmalıdır (scattering) ve geçiş kayıpları yine olabildiğince az olmalıdır.
- Dieltrik malzemede yapılmalıdır. İletken olamaz. Polypropilen
- Bir radomda dalgaların, hem gidiş ve hem de geliş yönündeki zayıflama oranları aynı olmalıdır. Bu nedenle bir "Çift Yönlü Zayıflama" söz konusudur. Bu Çift Yönlü Zayıflama değeri köpüklü bir malzemeden yapılmış bir radomda tipik 0,3 dB civarındadır, yani bu yüksek frekanslı enerjide yaklaşık bir toplam %7 lik kayba karşılık gelir. Radar denklemine göre ise bu yaklaşık %2 lik bir menzil kaybı demektir.
- Uçağın burnunda rüzgarı ilk karşılayan bölge olan radom, radar antenlerinin üzerine yapılan kaplama olarak özetlenebilir. Radom, uçağa aerodinamik bir özellik kazandırır.
- Ayrıca hızlı bir şekilde dönen antenler sayesinde yakındaki personeli kazara çarpmalara karşı korurlar.

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Kaynaklar

- https://www.ece.ucsb.edu/~long/ece145a/ampdesign.pdf
- Amplifiers, Prof. Tzong-Lin Wu. EMC Laboratory. Department of Electrical Engineering. National Taiwan University

Usage Notes

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